

CHANIA2023

10th International Conference on
Sustainable Solid Waste Management

21-24 JUNE

ANALYSIS OF POSSIBILITIES OF OBTAINING POSITIVE ENERGY BALANCE IN ANAEROBIC DIGESTION SYSTEMS WITH HYDRODYNAMIC DISINTEGRATION

Monika Żubrowska-Sudoł, Katarzyna Sytek-Szmeichel,
Justyna Walczak, Agnieszka Garlicka, Katarzyna Umiejewska

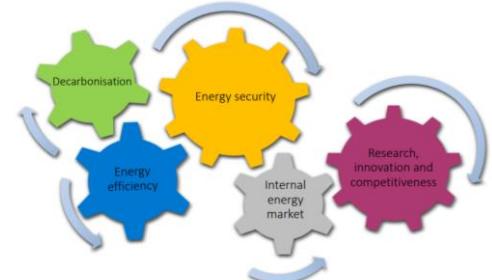
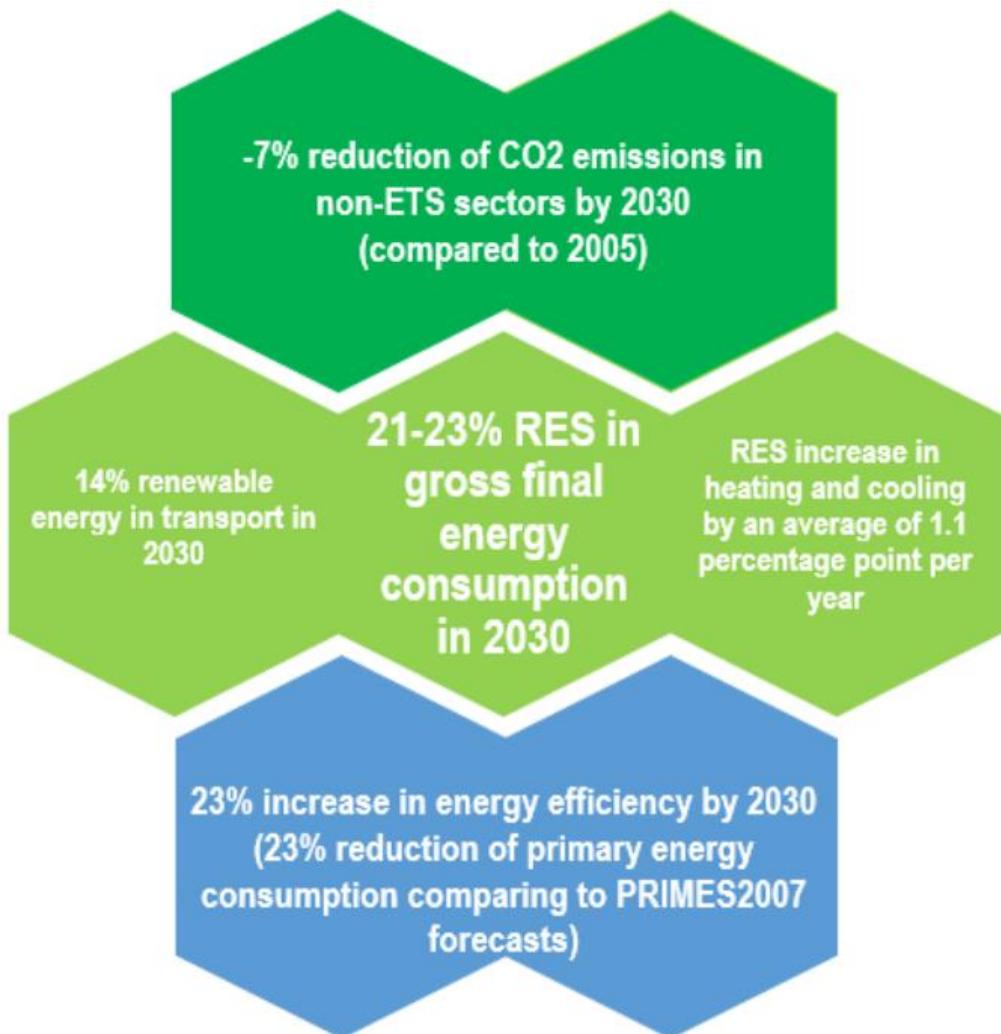
Warsaw University
of Technology



Faculty of Building
Services, Hydro and
Environmental Engineering
WARSAW UNIVERSITY OF TECHNOLOGY

„Development of a technology for preparation substrates used in methane co-fermentation by disintegration methods”
(DEZMETAN) No.: POIR.04.01.02-00-0022/17

POLAND'S NATIONAL ENERGY AND CLIMATE PLAN FOR THE YEARS 2021-2030

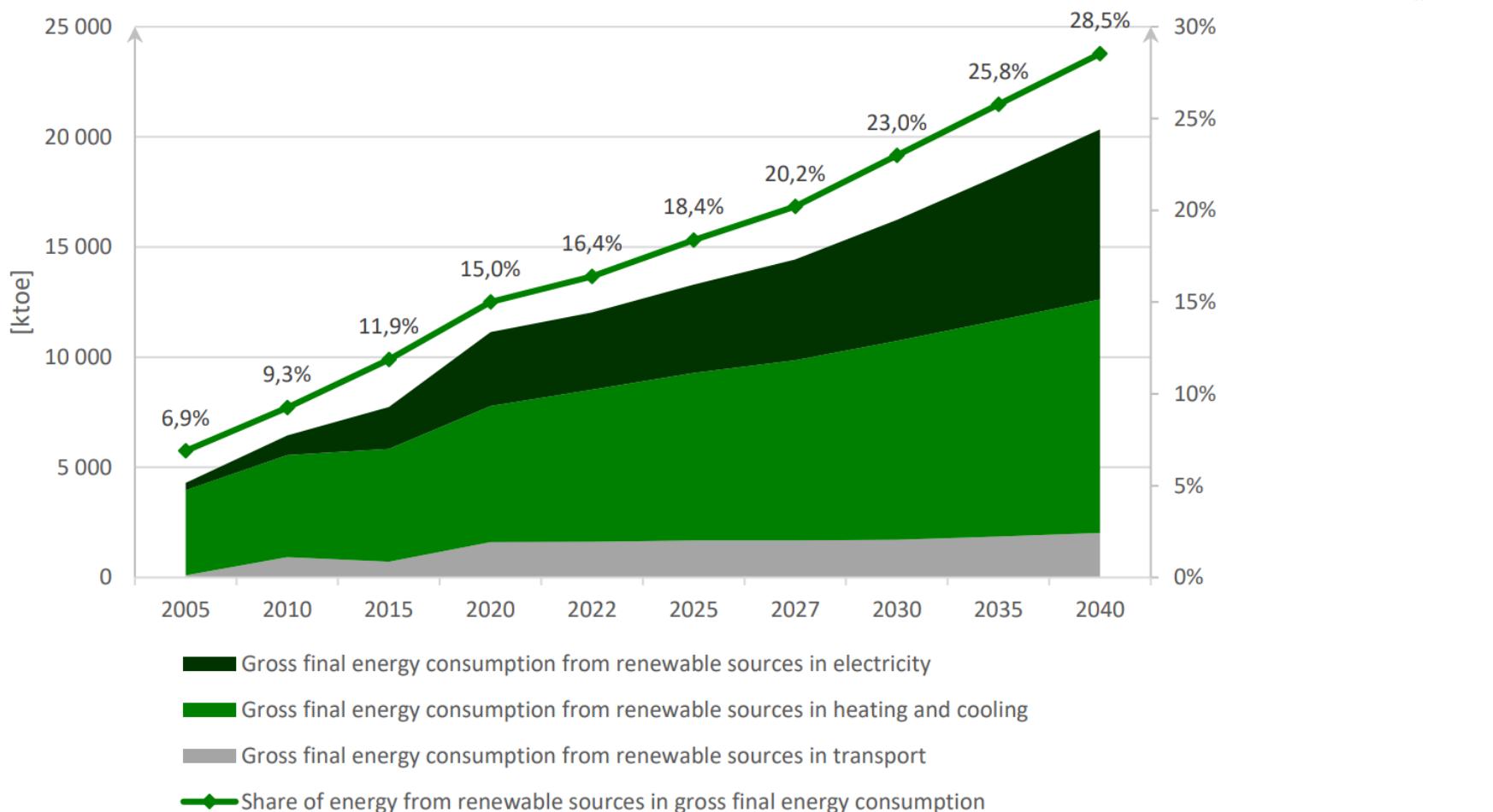
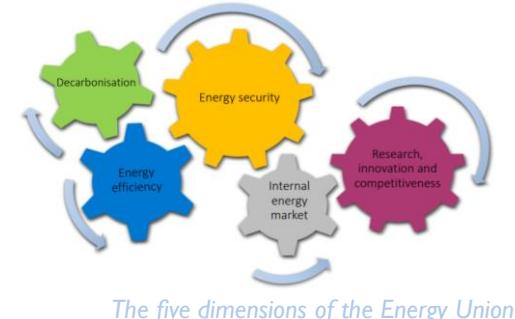


The five dimensions of the Energy Union

**Poland's climate
and energy targets
until 2030**

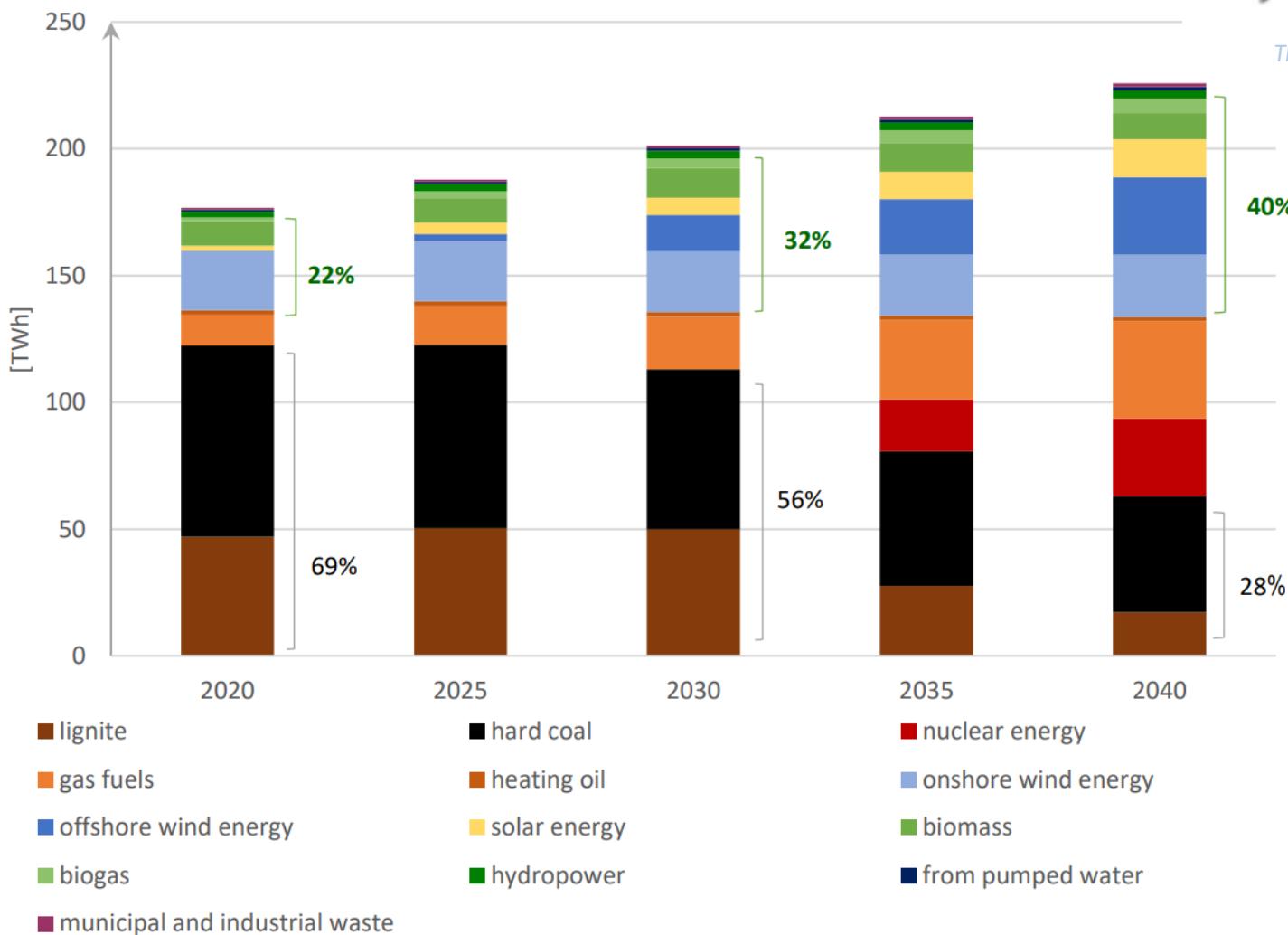
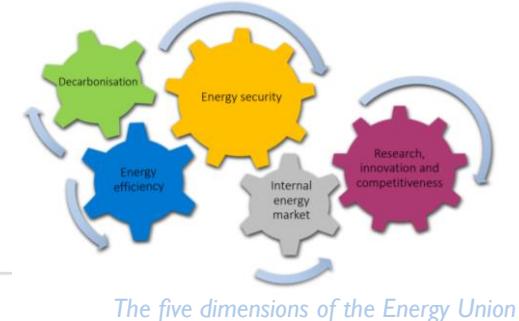
POLAND'S NATIONAL ENERGY AND CLIMATE PLAN FOR THE YEARS 2021-2030

Renewable Sources development



POLAND'S NATIONAL ENERGY AND CLIMATE PLAN FOR THE YEARS 2021-2030

Structure of electricity production



RESEARCH PROBLEM

How to increase biogas production?

Pretreatment

e.g. disintegration process

ENERGY

(mechanical, thermal, chemical)



increasing the availability of the substrate for microorganisms involved in the anaerobic digestion process

Co-digestion process

Substrate

(e.g. sewage sludge)



Co-substrate

characterized by a high methane production potential



increase of calorific value of substrates entering the anaerobic digester

Article

Energy-Positive Disintegration of Waste Activated Sludge—Full Scale Study

Monika Zubrowska-Sudol^{1,*}, Katarzyna Sytek-Szmeichel¹, Piotr Krawczyk² and Agnieszka Bisak¹

- ¹ Faculty of Building Services, Hydro and Environmental Engineering, Warsaw University of Technology, Nowowiejska 20, 00-653 Warsaw, Poland; katarzyna.szmeichel@pw.edu.pl (K.S.-S.); agnieszka.bisak@gmail.com (A.B.)
² Faculty of Power and Aeronautical Engineering, Warsaw University of Technology, Nowowiejska 24, 00-655 Warsaw, Poland; piotr.krawczyk@pw.edu.pl
* Correspondence: monika.sudol@pw.edu.pl

Abstract: This study aimed to evaluate the effects of mechanical disintegration of waste activated sludge (WAS) on full scale anaerobic digestion, considering the possibility of obtaining a positive energy balance. The results showed that an increase in energy density (ϵ_L) used in disintegration was accompanied by an increase in the release of organic compounds from sludge (SCOD increased from 211 ± 125 mg O₂/L for $\epsilon_L = 0$ kJ/L to 6292 ± 2860 mg O₂/L for $\epsilon_L = 180$ kJ/L). Some of them were volatile fatty acids. The percentage share of WAS subject to disintegration was also documented as a crucial parameter affecting the efficiency of biogas production. An increase in the value of this parameter from 25% to 100%, even at much lower ϵ_L used in disintegration (therefore with much smaller amounts of organic compounds released from sludge flocs) resulted in an increase in biogas

Bioresource Technology 360 (2022) 127622

Contents lists available at ScienceDirect

Bioresource Technology

journal homepage: www.elsevier.com/locate/biores

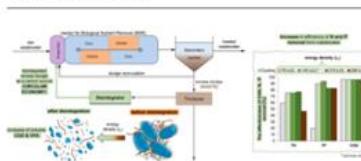
Disintegration of waste sludge as an element bio-circular economy in waste water treatment plant towards carbon recovery for biological nutrient removal

Monika Zubrowska-Sudol¹, Justyna Walczak¹, Grzegorz Piechota²¹ Faculty of Building Services, Hydro and Environmental Engineering, Warsaw University of Technology, Nowowiejska 20, 00-653 Warsaw, Poland;² GCPHM, Laboratory of Biogas Research and Analysis, ul. Legionów 40a/3, 87-100 Turek, Poland

HIGHLIGHTS
• Recovery economy of excess sludge via disintegration process was investigated.
• Disintegrated excess sludge as a source of C to increase N and P removal was used.

• N and P removal depended on energy densities at which C was produced.
• Increase of energy density of C produced was observed at 70 kJ/L and 210 kJ/L.
• Decline in efficiency of N and COD removal was observed at 280 kJ/L.

GRAPHICAL ABSTRACT



ABSTRACT

The goal of the study was to evaluate the possibility of use of disintegrated excess sludge to enhance combined biological nutrient removal from wastewater. In the experiments lasting 295 days four runs were performed.

RESEARCH PAPER

Water

CLEAN

Soil Air Water

www.clean-journal.com

Influence of Hydrodynamic Disintegration on the Release of Organic and Nutrient Compounds From Activated Sludge

Justyna Walczak^{*}, Monika Zubrowska-Sudol, and Paula Piechota

The aim of the research is to assess the release of organic compounds and nutrients to liquid phase as a result of hydrodynamic disintegration (HD) of sludge. Six batch disintegration tests are conducted. The scope is a complex analysis of the release of organic compounds (soluble chemical oxygen demand [SCOD], volatile fatty acids [VFA] and nutrients (soluble total nitrogen [STN], NO_x–N, NO₂–N, NH₄–N, soluble total phosphorus [STP], PO₄³⁻-P) depending on the energy density (ϵ_L) used during the HD process (70–350 kJ/L). It is shown that an increase in ϵ_L is correlated with an increase in the disintegration degree (DO). This results in an increase in both the SCOD (including VFA) and in the soluble nutrient concentration (STN and STP). The value of ϵ_L , at which HD is conducted, also has an influence on the percentage share of VFA in soluble organic compounds released from activated sludge flocs and on the relationship between the SCOD/STN and SCOD/STP ratio. It is also shown that ϵ_L and the total solids concentration of disintegrated sludge have an influence on the costs of organic compounds acquired by the HD method. Low costs are obtained for $\epsilon_L = 350$ kJ/L (0.7–2.2 kg⁻¹ SCOD and 12.8–21.64 kg⁻¹ VFA), and for relatively high total solids (TS) concentrations (TS > 4%) (1.5–1.9 kg⁻¹ SCOD for $\epsilon_L = 70$ kJ/kg and 0.7–0.8 kg⁻¹ SCOD for $\epsilon_L = 350$ kJ/L).

production and to percentage reduction of volatile total solids (VTS). Moreover, disintegrated excess sludge has higher calorific value than raw sludge. Sludge disintegration is also referred to as a method of obtaining an alternative carbon source for intensifying nutrient removal from wastewater.

There are many ways of conducting sludge disintegration, and they differ by the source of energy entering the system, for example, mechanical ballast, ball mill homogenization, pressure methods, hydrodynamic disintegration (HID) [1,2,8–11], physical (high temperature) [12,13], chemical (ozone treatment) [14,15] and biological [16]. A combination of two or more methods is also used [17]. In practice, the choice of disintegration method is dictated by the required disintegration efficiency and, above all, by the investment and operational costs of the system. In order to conduct a comparison of energy input parameters were introduced in the disintegration process, called: energy density



ELSEVIER

MDPI

Effect of hydrodynamic disintegration on the solubilisation and bioavailability of thickened excess sludge

Agnieszka Garlicka¹, Monika Zubrowska-Sudol¹

Department of Water Supply and Wastewater Treatment, Faculty of Building Services, Hydro and Environmental Engineering, Warsaw University of Technology, Nowowiejska 20, 00-653 Warsaw, PL, Poland

ARTICLE INFO

Keywords:
 Bioavailability
 COD stabilisation
 hydrolysis
 hydrodynamic disintegration
 thickened excess sludge
 wastewater engineering

ABSTRACT

The main objective of the study was the verification whether conducting the hydrodynamic of thickened excess sludge (TES) before the anaerobic hydrolysis (AH) can cause an increase in the hydrolysis process, and therefore a reduction in its duration, or allow for complete CH_4 production. For this purpose, the HD (conducted in five levels of energy density: 140, 280, 420, 560 and 700 kJ/L) of TES was carried out, and then all sludges (before and after subjected to the AH). The obtained results confirmed that the process of HD can be a



Contents lists available at ScienceDirect

Thermal Science and Engineering Progress

journal homepage: www.elsevier.com/locate/tsep



The effects of mechanical sludge disintegration to enhance full-scale anaerobic digestion of municipal sludge

Monika Zubrowska-Sudol^{1,*}, Jolanta Podędowna², Katarzyna Sytek-Szmeichel¹,Agnieszka Bisak³, Piotr Krawczyk³, Agnieszka Garlicka¹¹ Warsaw University of Technology, Faculty of Building Services, Hydro and Environmental Engineering, 20 Nowowiejska Str., 00-653 Warsaw, Poland² Warsaw University of Technology, Faculty of Power and Aeronautical Engineering, 24 Nowowiejska Str., 00-655 Warsaw, Poland

ARTICLE INFO

Keywords:
 Anaerobic digestion
 Mechanical disintegration
 Waste activated sludge
 Biogas production

ABSTRACT

The main goal of the study was to evaluate the effects of mechanical sludge disintegration in enhancing full-scale anaerobic digestion of municipal sludge. Batch disintegration tests and lab-scale testing tests were performed to determine the release of organic compounds and to assess the impact of disintegration of excess sludge before the fermentation process on the sludge and the digestibility of post-fermented sludge, respectively. In the study, a disintegration driven by a high energy density was used. It was found that increased amounts of organic compounds were released from the sludge along with an increase in energy consumed in the disintegration. A part of the organic compounds were volatile fatty acids (VFAs). The highest share of VFAs in the released organic compounds (COD/VFA in the range of 6.6 ± 8.2) was obtained by performing disintegration at an energy density of 140 kJ/L. It was also determined that the introduction of excess sludge to the reactor significantly increases the share of VFAs in the released organic compounds (an average of 33.9%) and an increase in volatile total solids reduction in the fermented sludge by an average of 22.7%. Such a surplus of produced biogas would allow to produce ca. 1600 kWh/d of electricity and 7.5 GJ/d (2010 kWh/d) of heat. Moreover, it was determined that the share of disintegrated waste activated sludge in the mixed sludge subjected to the fermentation process could considerably influence the efficiency of post-fermented sludge digesting.



energies

Article

Effects of Thickened Excess Sludge Pre-Treatment Using Hydrodynamic Cavitation for Anaerobic Digestion

Agnieszka Garlicka^{1,*}, Monika Zubrowska-Sudol¹, Katarzyna Umięjewska¹, Otton Roubinek², Jacek Palige² and Andrzej Chmielewski¹¹ Department of Water Supply and Wastewater Treatment, Faculty of Building Services, Hydro and Environmental Engineering, Warsaw University of Technology, 20 Nowowiejska Str., 00-653 Warsaw, Poland; monika.sudol@pw.edu.pl (M.Z.-S.); katarzyna.umiejewska@pw.edu.pl (K.U.)² Institute of Nuclear Chemistry and Technology, 16 Dziedzicza St., 03-195 Warsaw, Poland; o.roubinek@ichf.edu.pl (O.R.); j.palige@ichf.edu.pl (J.P.); a.chmielewski@ichf.edu.pl (A.C.)^{*} Correspondence: agnieszka.garlicka.dok@pw.edu.pl

Received: 17 April 2020; Accepted: 12 May 2020; Published: 14 May 2020

Abstract: The main purpose of this study was the assessment of the possibility of increasing the production of biogas through the pre-treatment of thickened excess sludge (TES) by means of the hydrodynamic cavitation (HC) conducted at different levels of energy densities (E), i.e., 70, 140, and



Article

Energy-Positive Disintegration of Waste Activated Sludge—Full Scale Study

Monika Zubrowska-Sudol ^{1,*}, Katarzyna Sytek-Szmeichel ¹, Piotr Krawczyk ² and Agnieszka Bisak ¹

- ¹ Faculty of Building Services, Hydro and Environmental Engineering, Warsaw University of Technology, Nowowiejska 20, 00-653 Warsaw, Poland; katarzyna.smiechek@pw.edu.pl (K.S.-S.); agnieszka.buski@gmail.com (A.B.)
² Faculty of Power and Aeronautical Engineering, Warsaw University of Technology, Nowowiejska 24, 00-655 Warsaw, Poland; piotr.krawczyk@pw.edu.pl
^{*} Correspondence: marta.sudo@pw.edu.pl

Abstract: This study aimed to evaluate the effects of a 3D-printed dental implant abutment developed by VSP® on full-arch support function, which can reduce the risk of bone loss and improve the long-term clinical performance of dental implants.

...excess biogas obtained due to the disintegration process would allow for producing an amount of electricity higher than that used for pre-treatment method

Disintegration
water treatment
nutrient remo.

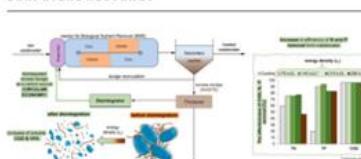
Monika Zubrowska-

第二步：选择合适的定价策略

1000-1000

- Biocircular economy of excess sludge via disintegration process was investigated.
 - Disintegrated excess sludge as a source of C to increase N and P removal was used.
 - N and P removal depended on energy densities at which C was produced.
 - Increase of combined N and P removal was obtained at 70 kJ/L and 210 kJ/L.
 - Decline in efficiency of N and COD removal was observed at 280 kJ/L.

GRAPHICAL ABSTRACT



ABSTRACT

The goal of the study was to evaluate the possibility of use of disintegrated excess sludge to enhance combined biological treatment processes. In this investigation, 20% dry weight excess sludge was added to the activated sludge system.

The aim of the research is to assess the release of organic compounds and nutrients to liquid phase as a result of hydrodynamic disintegration (HD) of sludge. Six batch disintegration tests are conducted. The scope is a complex analysis of the release of organic compounds [soluble chemical oxygen demand (SCOD), volatile fatty acids (VFA) and nutrients (soluble total nitrogen (STN), NO_x^- , NH_4^+ , NH_3 , soluble total phosphorus (STP), PO_4^{3-}] depending on the energy density (ϵ_{L}) used during the HD process (70–350 J L^{-1}). It is shown that an increase in ϵ_{L} is correlated with an increase in the disintegration degree (DD). This results in an increase in both the SCOD (including VFA) and the soluble nutrient concentration (STN and STP). The value of ϵ_{L} , at which HD is conducted, also has an influence on the percentage share of VFA in soluble organic compounds released from activated sludge flocs and on the relationship between the SCOD/STN and SCOD/STP ratio. It is also shown that ϵ_{L} and the total solid concentration of disintegrated sludge have an influence on the cost of organic compounds acquired by the HD method. Low costs are obtained for $\epsilon_{\text{L}} = 350 \text{ J L}^{-1}$ ($0.7 \pm 2.2 \text{ g L}^{-1}$ SCOD and $12.8 \pm 23.64 \text{ mg L}^{-1}$ VFA), and for relatively high total solids (TS) concentrations ($\text{TS} > 45\%$) ($1.5 \pm 1.9 \text{ g L}^{-1}$ SCOD for $\epsilon_{\text{L}} = 70 \text{ J L}^{-1}$ and $0.7 \pm 0.4 \text{ g L}^{-1}$ SCOD for $\epsilon_{\text{L}} = 350 \text{ J L}^{-1}$).

production and to percentage reduction of volatile total solids (VTS).^{2,3} Moreover, disintegration can improve sludge dewaterability.⁴ Sludge disintegration is also referred to as a method of obtaining an alternative carbon source for intensifying nutrient removal from wastewater.^{5,6,7}

There are many ways of conducting sludge disintegration, and they differ by the source of energy entering the system. For example, mechanical (ultrasonics, shear mills, homogenization, pressure methods), hydrodynamic disintegration (HDS), physical (high temperature),^{8,9} chemical (hydrolysis, coarse treatment),¹⁰⁻¹² or biological^{13,14}. A combination of two or more methods is also used.¹⁵ In practice, the choice of disintegration method is dictated by the required disintegration efficiency and, alternatively, by the investment and operational costs of the system. In order to conduct a comparison of energy inputs, parameters were introduced in the disintegration, *versus*, *effected*, *densities*.

Strengthened Excess Sludge Pre-Treatment Using hydrodynamic Cavitation for Anaerobic Digestion

Agnieszka Garlicka ^{1,*}, Monika Zubrowska-Sudol ¹, Katarzyna Umiejewska ¹,
Ottón Roubinek ², Jacek Palusz ² and Andrzej Chmielewski ²

Department of Water Supply and Water-works Treatment Faculty of Built Environment

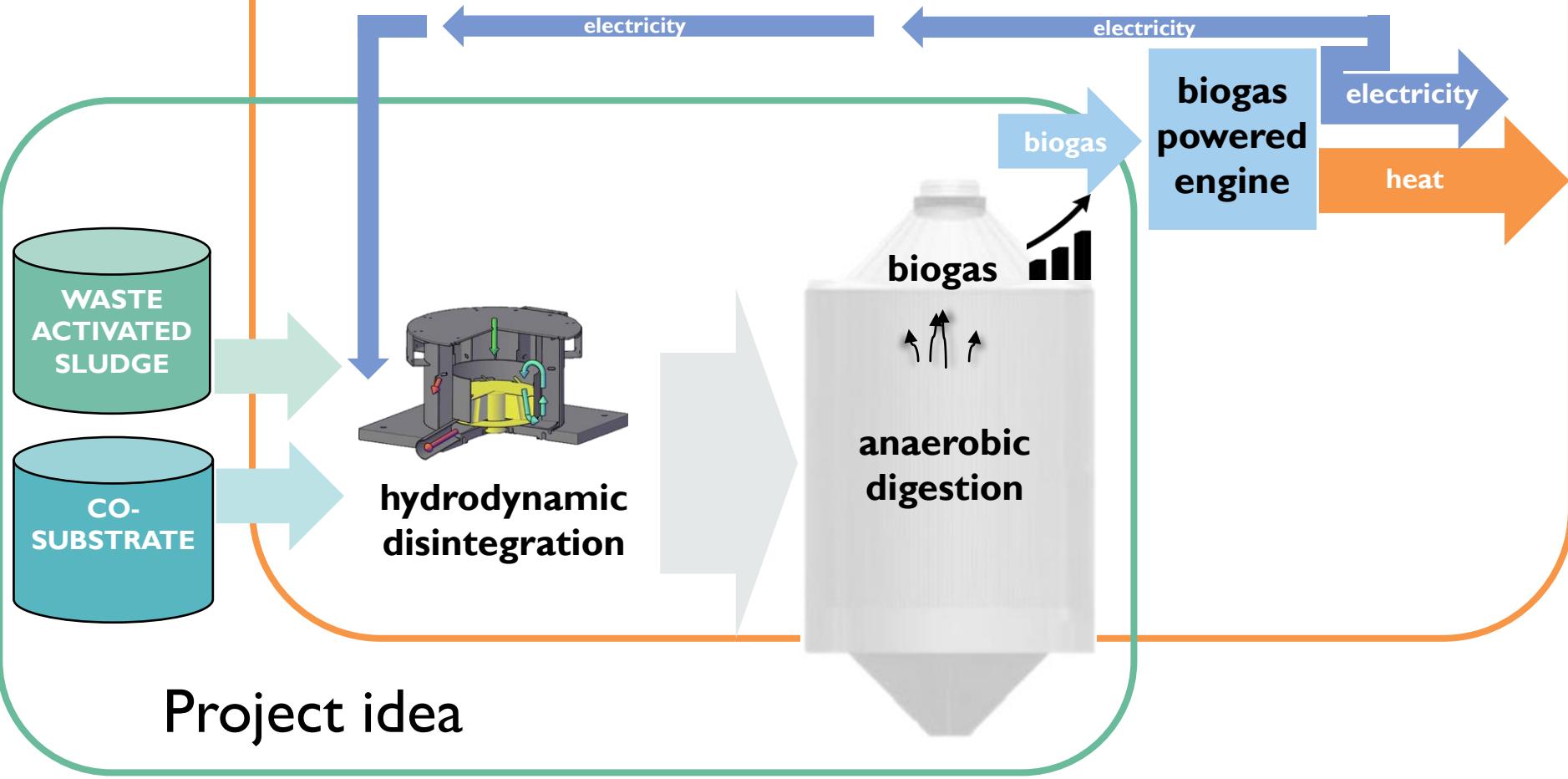
- ¹ Department of Water Supply and Wastewater Treatment, Faculty of Building Services, Hydro and Environmental Engineering, Warsaw University of Technology, 20 Nowowiejska St., 00-663 Warsaw, Poland; mrosika.sudol@wp.edu.pl (M.-S.); katarzyna.umiejsciwka@wp.edu.pl (K.U.)
² Institute of Nuclear Chemistry and Technology, 16 Dzerzinsk St., 03-195 Warsaw, Poland; o.roubinek@ichf.waw.pl (O.R.); paligej@ichf.waw.pl (P.J.); a.chmielewski@ichf.waw.pl (A.C.)
³ Correspondence: asemirja.ezakija.dokter@wp.edu.pl

Received: 17 April 2020; Accepted: 12 May 2020; Published: 14 May 2020

Abstract: The main purpose of this study was the assessment of the possibility of increasing the production of biogas through the pre-treatment of thickened excess sludge (TES) by means of the



Research challenge



„Development of a technology for preparation substrates used in methane co-fermentation by disintegration methods”
(DEZMETAN) No.: POIR.04.01.02-00-0022/17



Fundusze
Europejskie
Inteligentny Rozwój

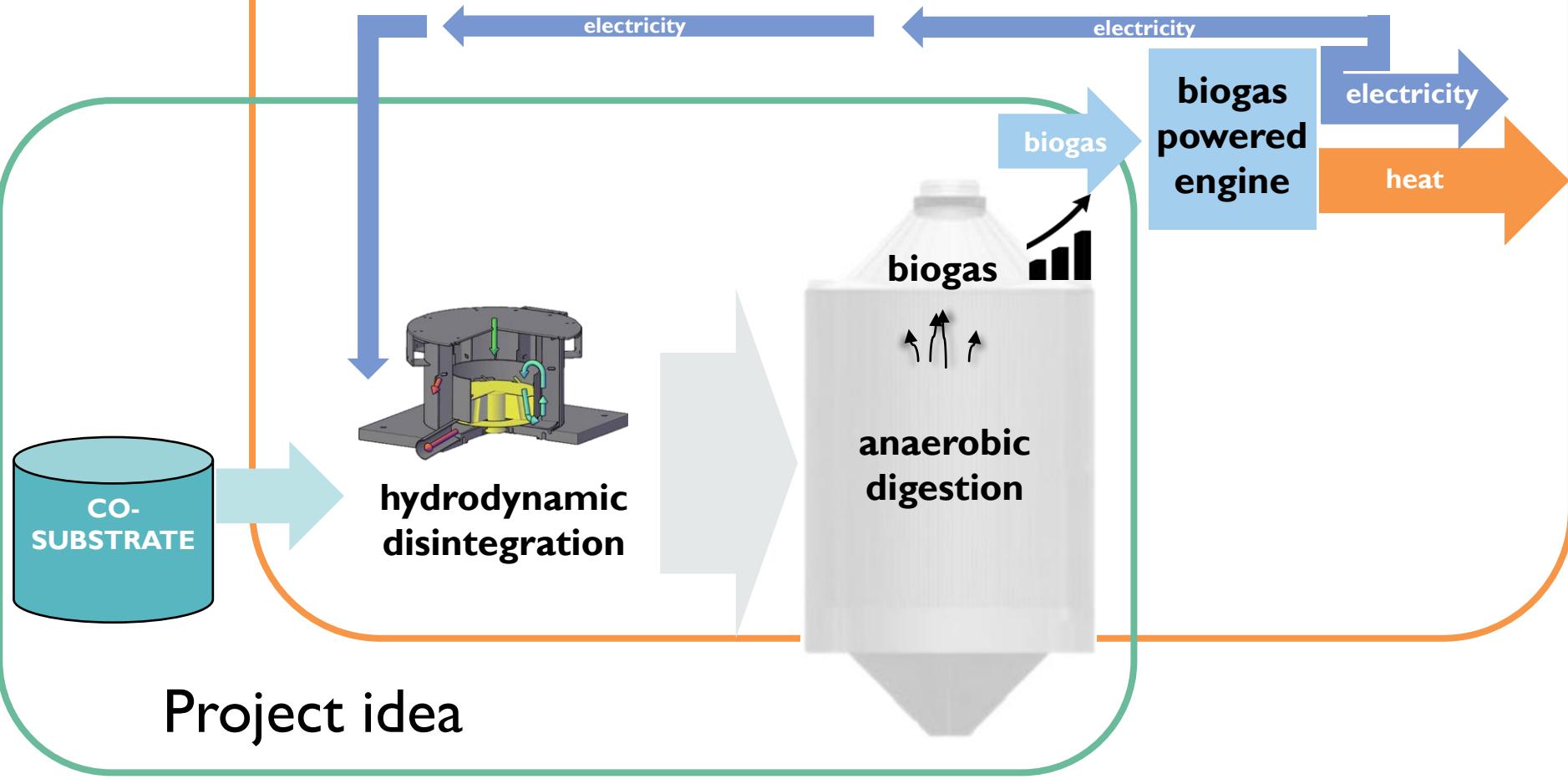


Narodowe Centrum
Badań i Rozwoju

Unia Europejska
Europejski Fundusz
Rozwoju Regionalnego



Research challenge



„Development of a technology for preparation substrates
used in methane co-fermentation by disintegration methods”
(DEZMETAN) No.: POIR.04.01.02-00-0022/17



Fundusze
Europejskie
Inteligentny Rozwój



Narodowe Centrum
Badań i Rozwoju

Unia Europejska
Europejski Fundusz
Rozwoju Regionalnego



AIM

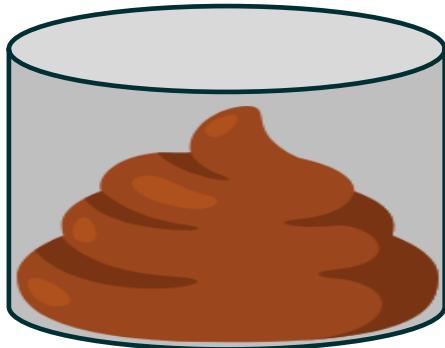
Analysis of the possibility of increasing the methane potential of selected co-substrates and obtaining a positive energy balance via hydrodynamic disintegration pre-treatment.

METHODS

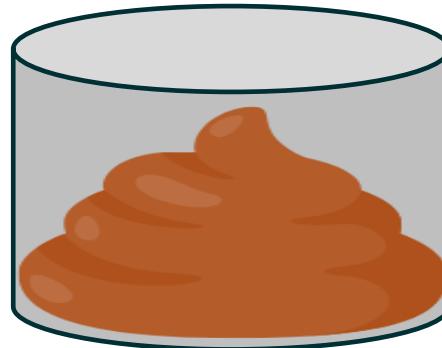


CO-SUBSTRATE

Cow manure CM
TS = 6.91 – 8.21 %



Pig manure PM
TS = 2.87 - 10.8 %



Maize silage MS
TS = 8.72 – 10.9 %



Remains of fruits RF
TS = 22.7 – 30.9 %



Beetroot pulp BP
TS = 9.16 – 19.4 %

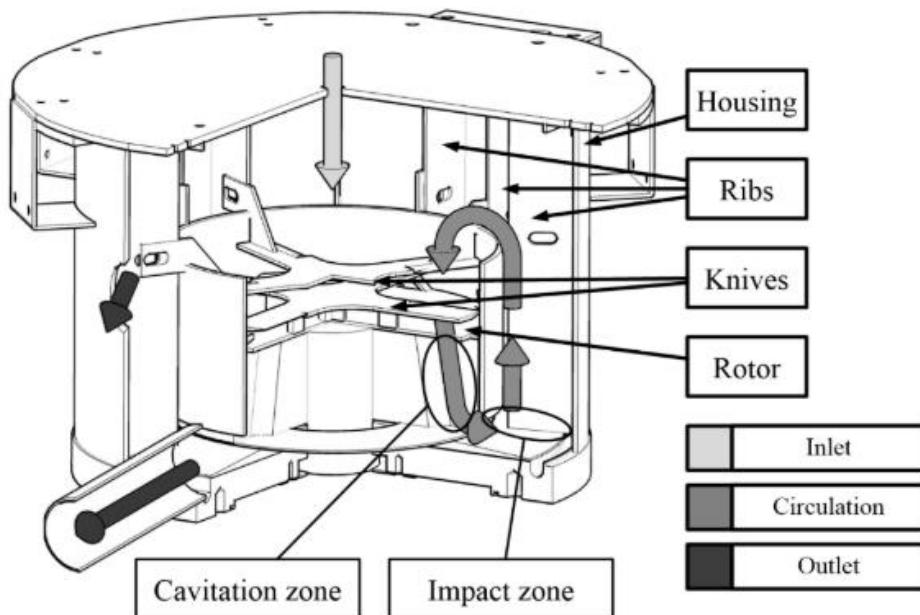


Beetroot pulp in the form of pellets BPP
TS = 87.6 – 94.0 %



HYDRODYNAMIC DISINTEGRATION

Disintegration apparatus



- Motor power: 5.5 kW
- Rotor revolution: 3000/min
- Volume of tank: 13 L



hydrodynamic disintegrator
(patent application WP-84/JW I3766I18)

Biochemical Methane Potential Test (BMP test)



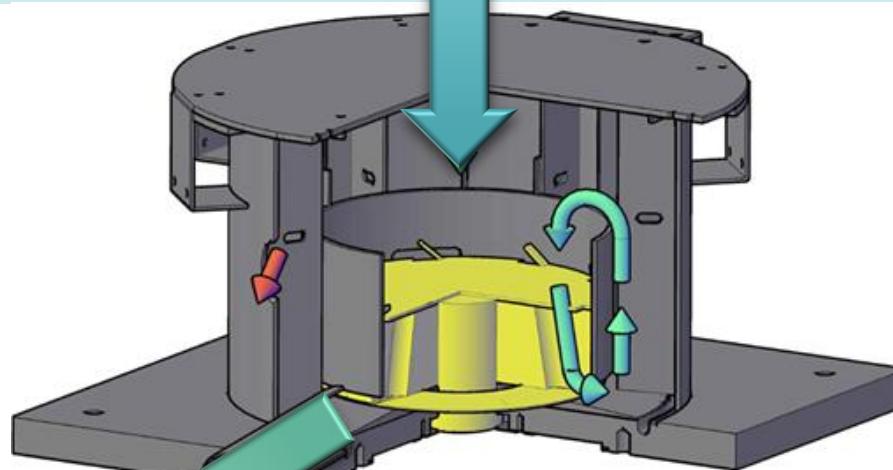
Specific Methane Production (SMP)

CO-SUBSTRATE
before
DISINTEGRATION

Biochemical Methane Potential Test (BMP test)



Specific Methane Production (SMP)



BMP test



SMP

CO-SUBSTRATE
after
DISINTEGRATION

BMP test



SMP

diluted to TS \approx 5 % (MS, RF, BP, BPP)

Biochemical Methane Potential Test (BMP test)

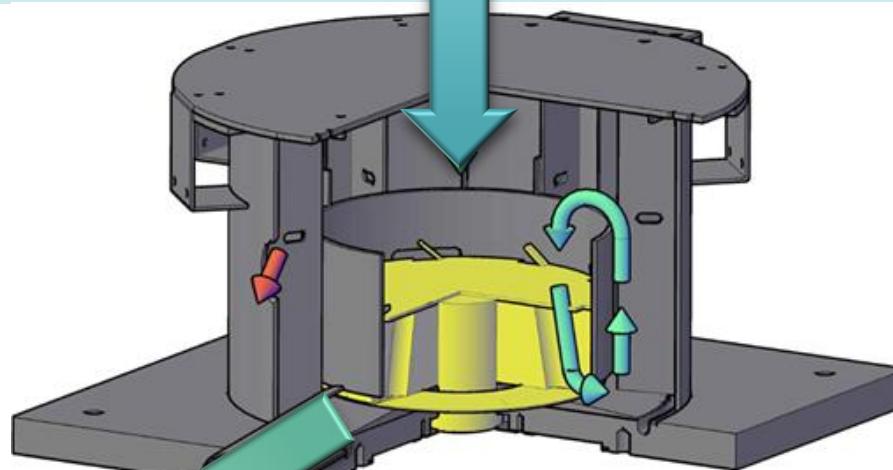


Specific Methane Production (SMP)

Biochemical Methane Potential Test (BMP test)



Specific Methane Production (SMP)



BMP test



SMP



BMP test



SMP

diluted to TS \approx 5 % (MS, RF, BP, BPP)

Biochemical Methane Potential Test (BMP test)



Specific Methane Production (SMP)

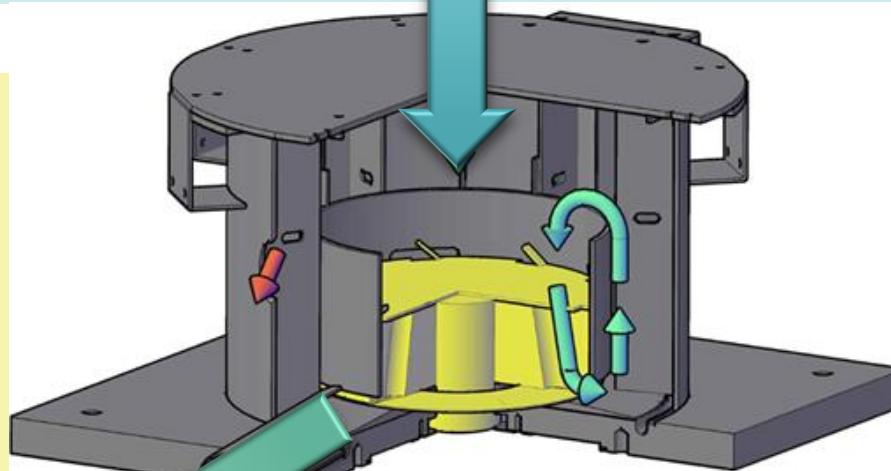
Biochemical Methane Potential Test (BMP test)



Specific Methane Production (SMP)

SERIES I

Energy density \mathcal{E}_L :
35 – 140 kJ/L



BMP test



SMP

SERIES 2

Energy density \mathcal{E}_L :
10 – 35 kJ/L



BMP test



SMP

Biochemical methane potential tests (BMP)

- constant temperature of 37°C
- initial organic loading rate 5 gVTS_{of introduced substrate}/L
- each assay was performed in three repetitions



Automatic Methane Potential Test System
(AMPTS II - Bioprocess Control Sweden)

Specific Methane Production (SMP)

Holliger,C., Alves,M., Andrade,D., Angelidaki,I., Astals,S., Baier,U., Ebertseder,F. et al.: Towards a standardization of biomethane potential tests. *Water Science and Technology* 74(11), 2515-2522 (2016)

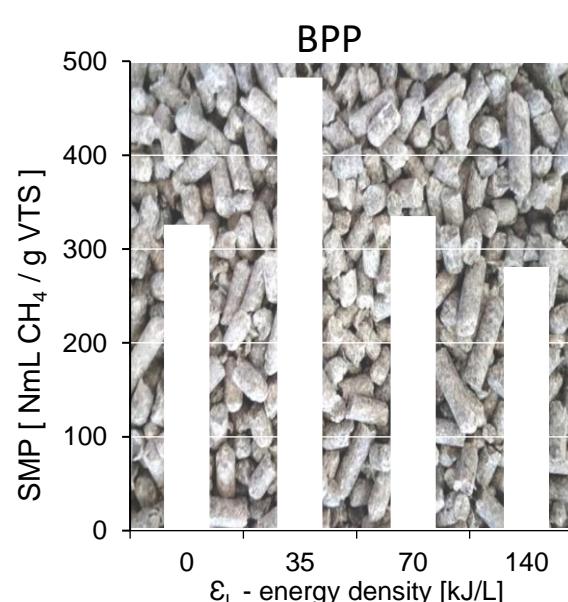
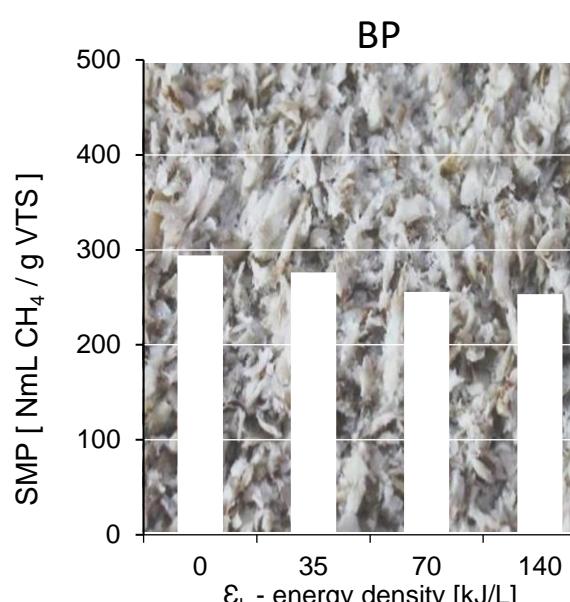
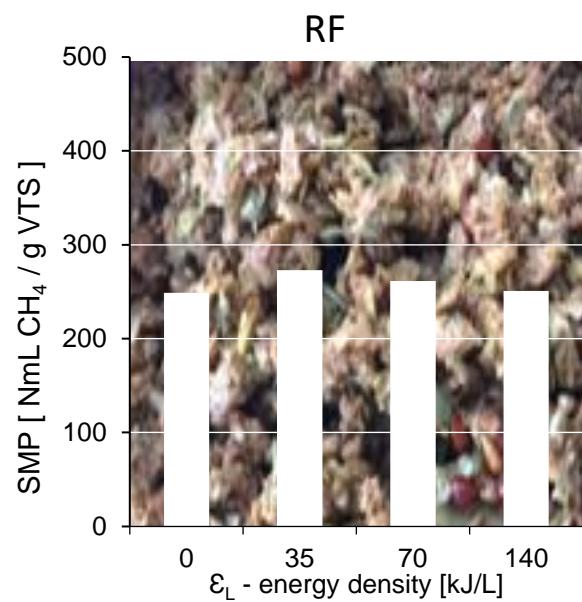
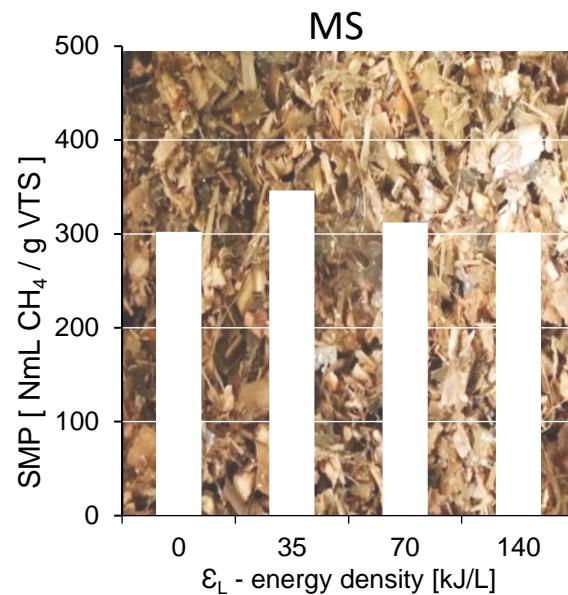
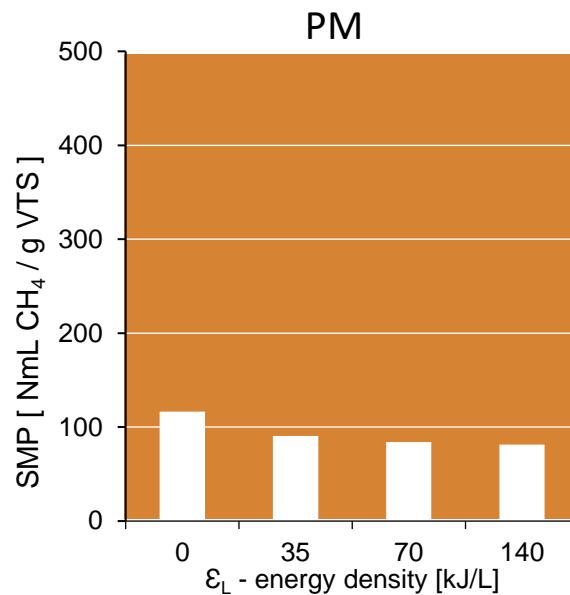
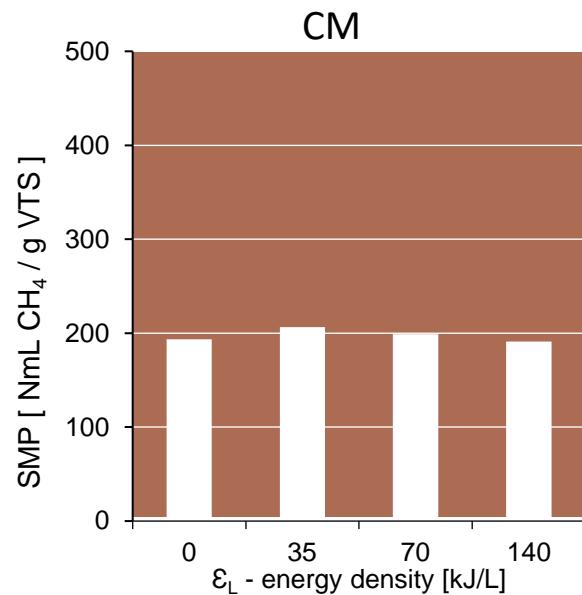
Zielinski M., Debowski M., Kisielewska M., Nowicka A., Rokicka M., Szwarc K.: Comparison of Ultrasonic and Hydrothermal Cavitation Pretreatments of Cattle Manure Mixed with Straw Wheat on Fermentative Biogas Production. *Waste Biomass Valor* 10, 747-754 (2019)

RESULTS



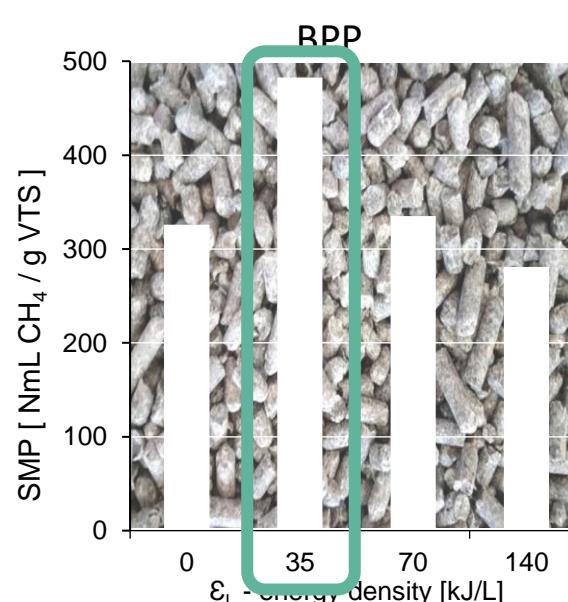
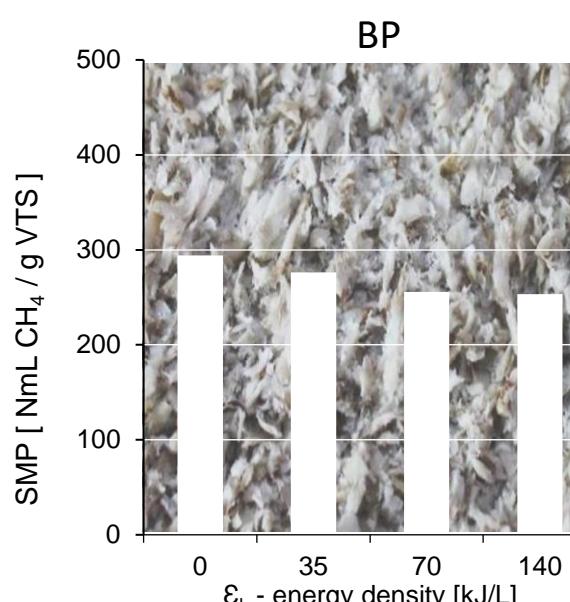
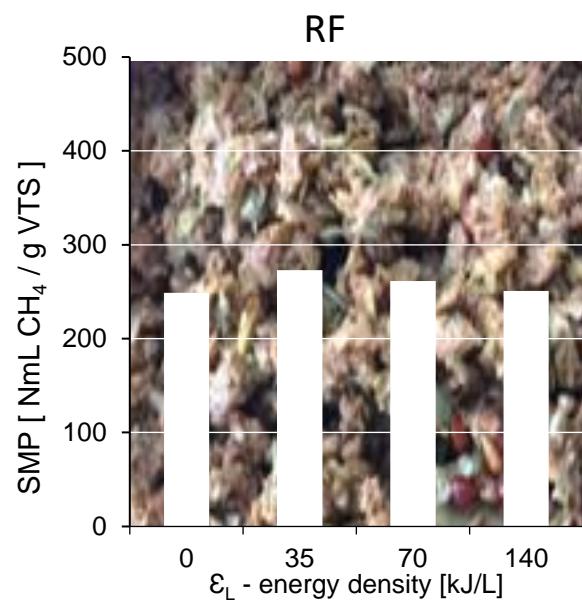
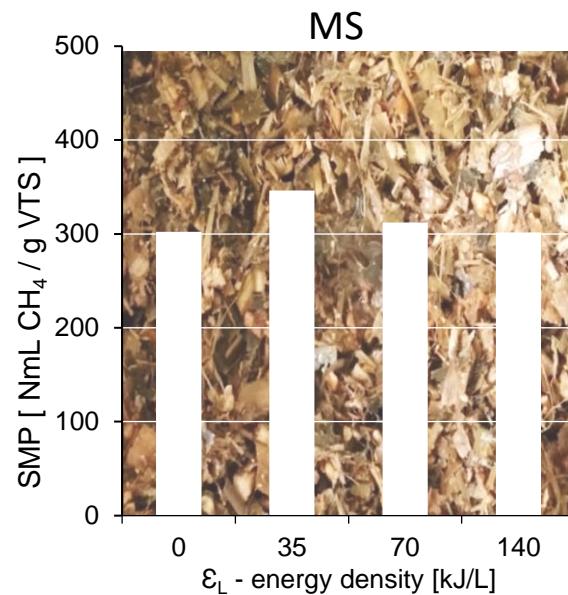
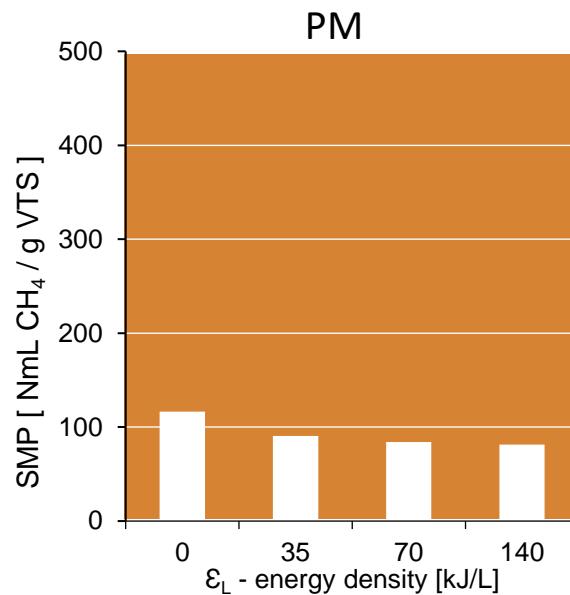
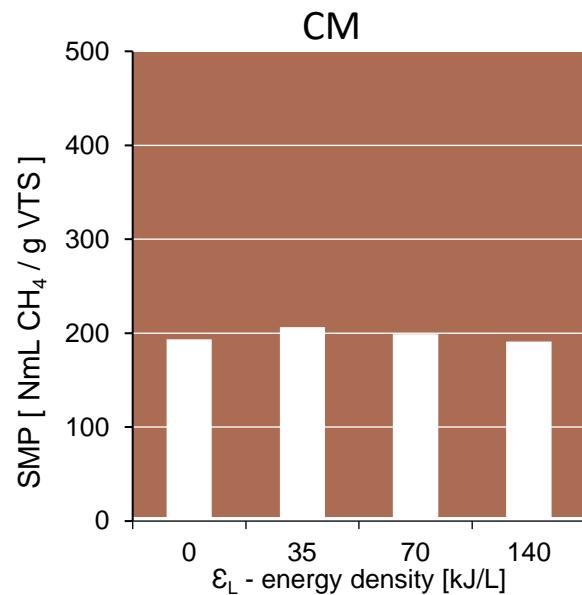
Biochemical methane potential (BMP) test

SPECIFIC METHANE PRODUCTION – SERIES I



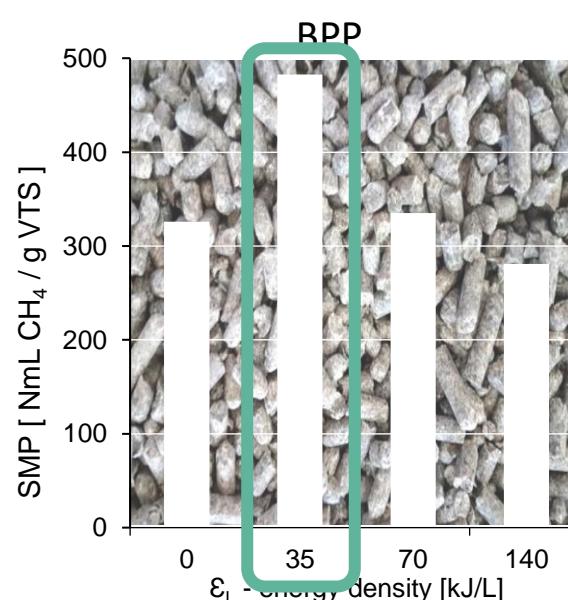
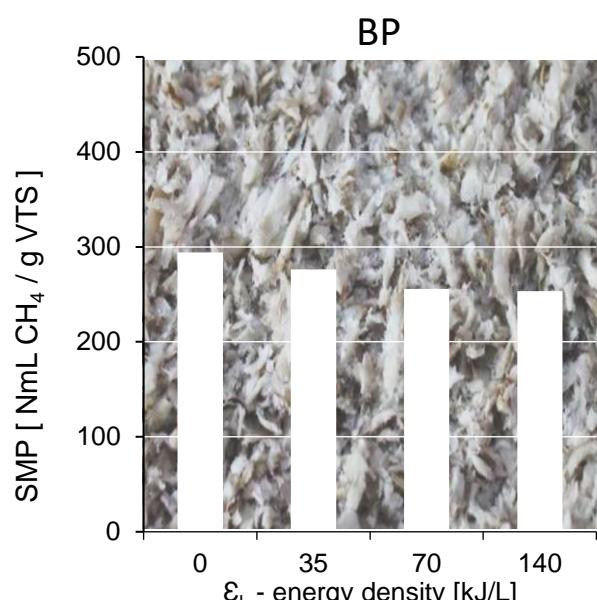
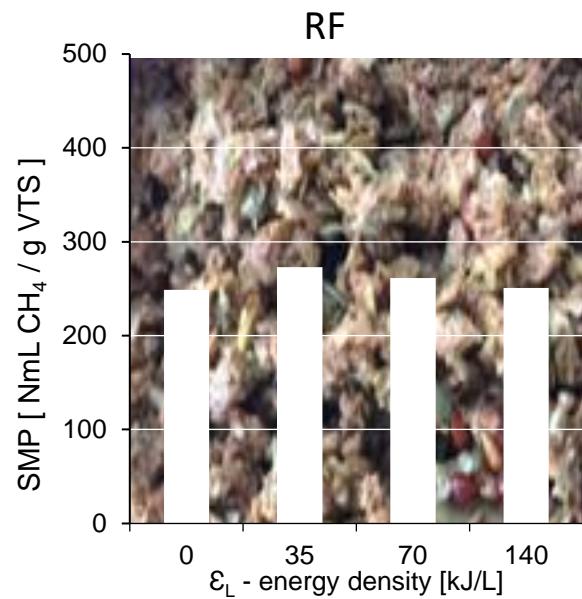
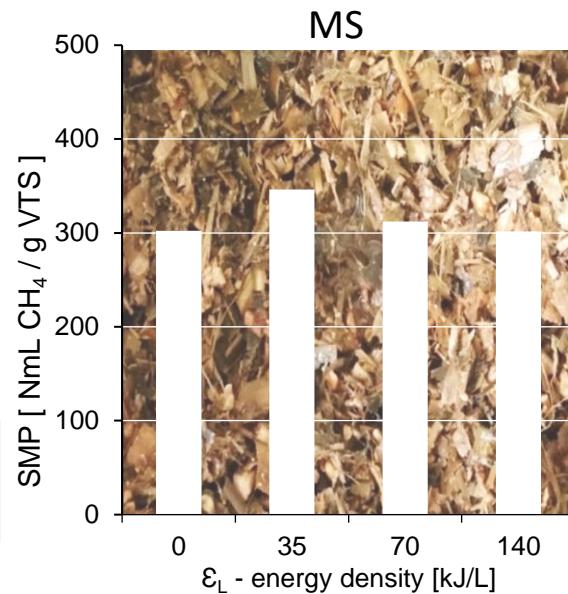
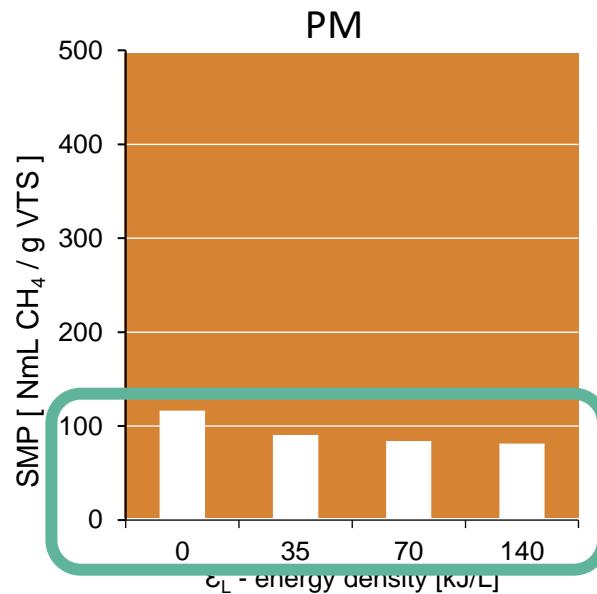
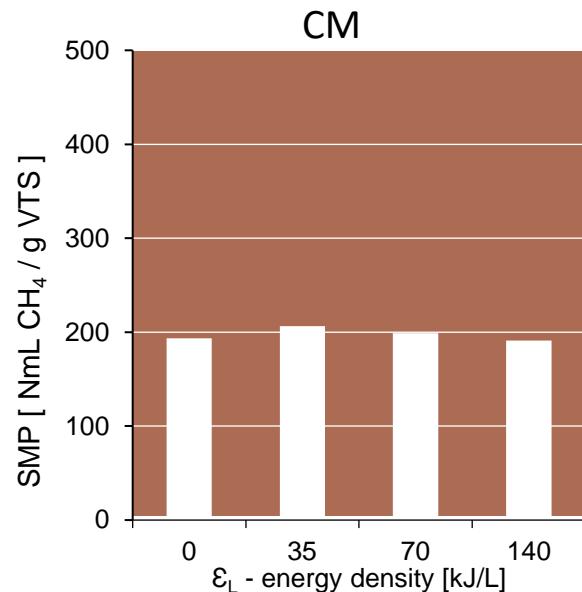
Biochemical methane potential (BMP) test

SPECIFIC METHANE PRODUCTION – SERIES I



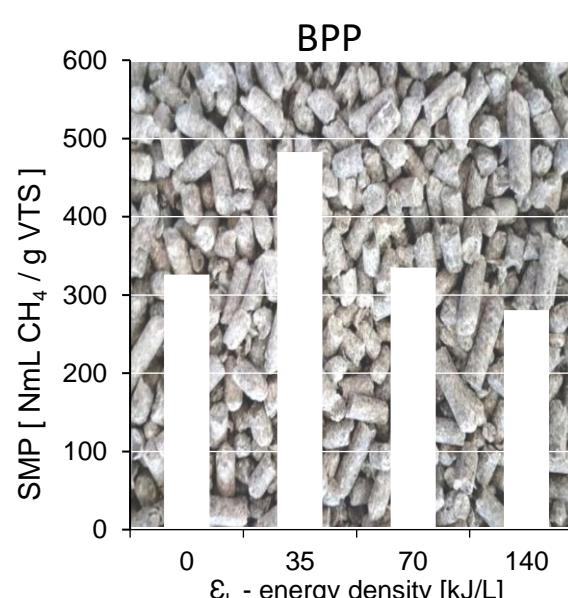
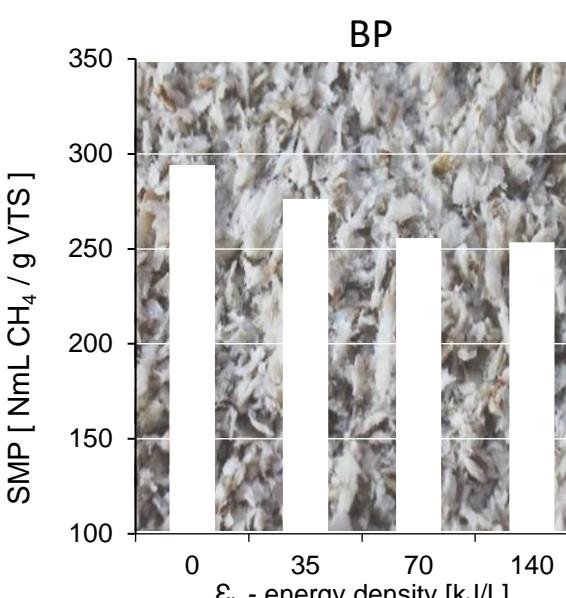
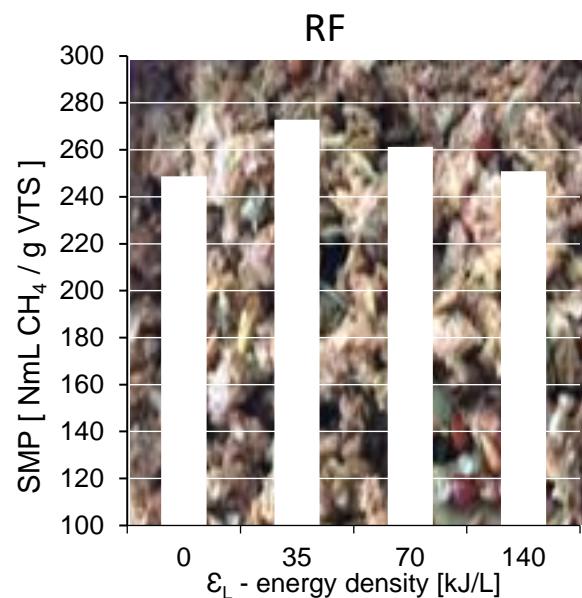
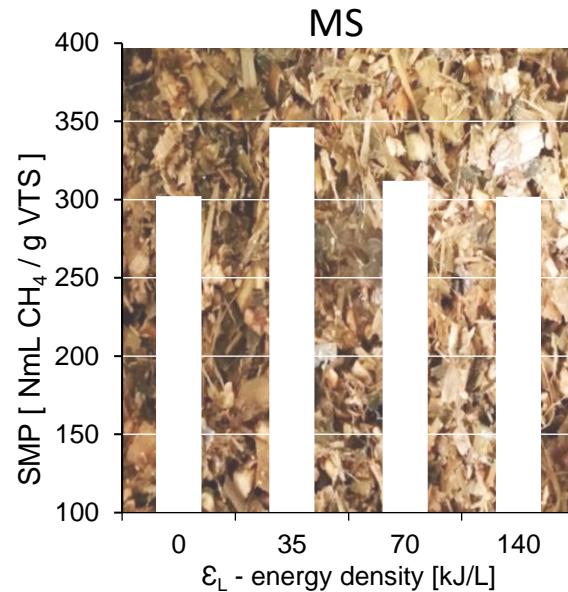
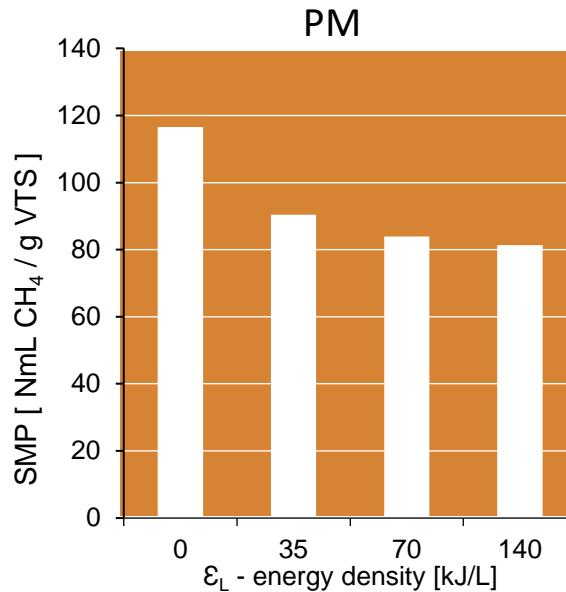
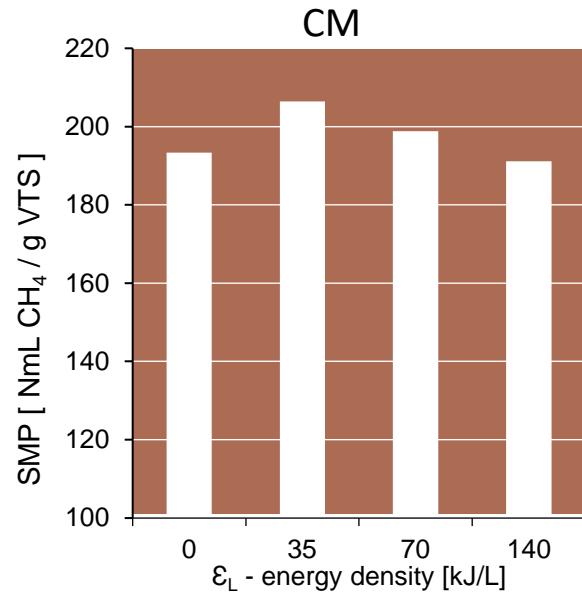
Biochemical methane potential (BMP) test

SPECIFIC METHANE PRODUCTION – SERIES I



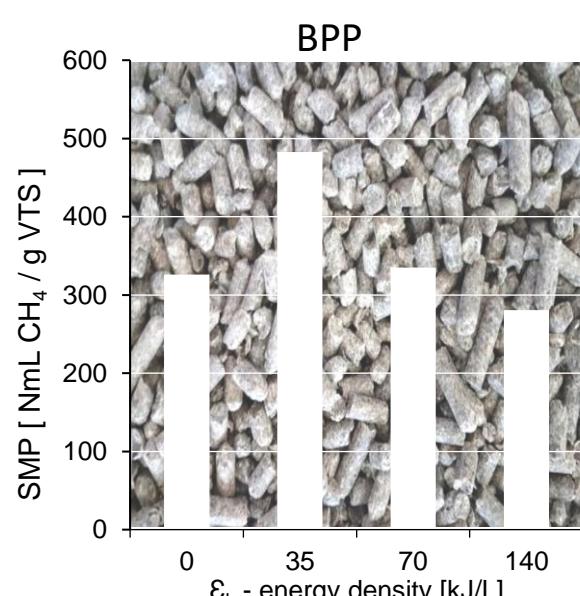
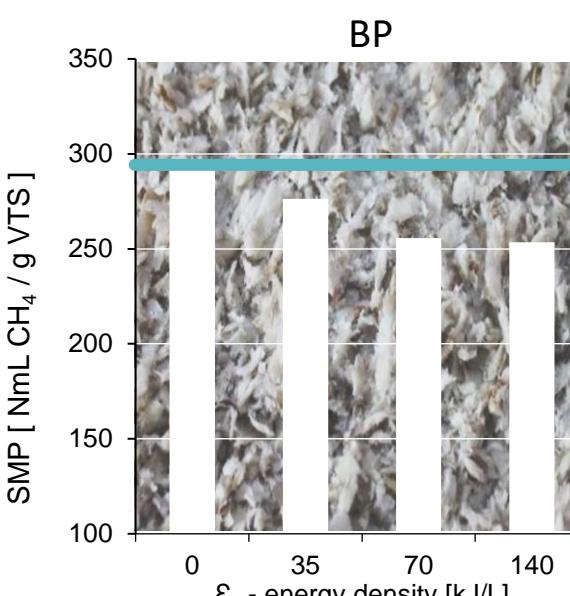
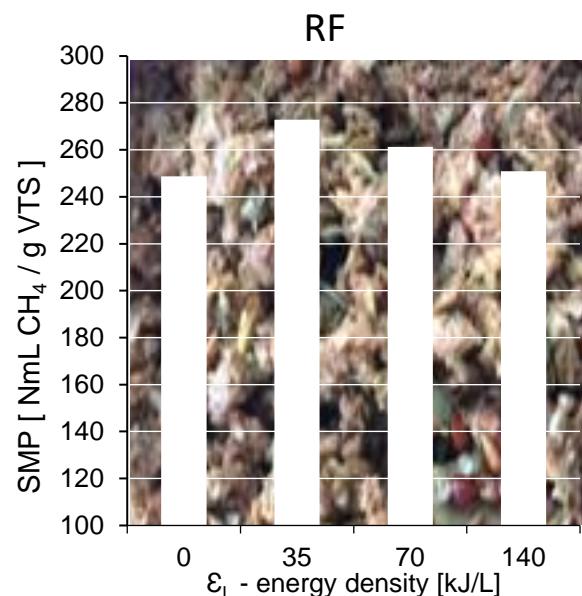
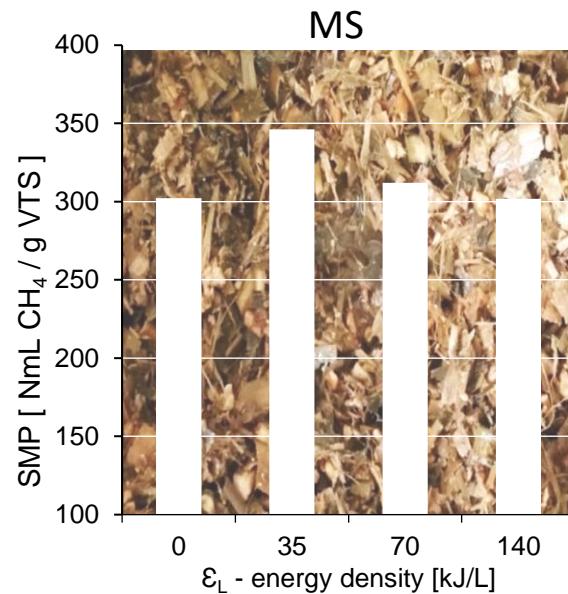
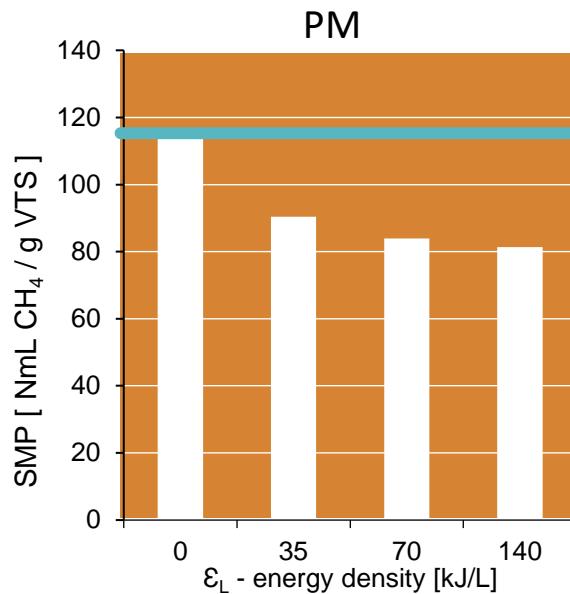
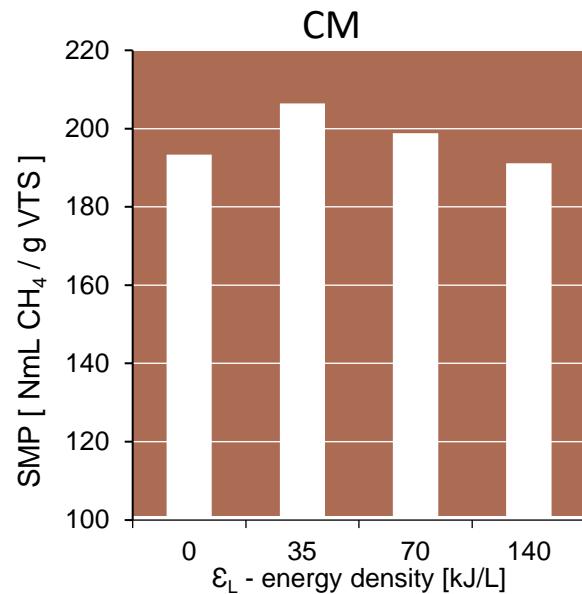
Biochemical methane potential (BMP) test

SPECIFIC METHANE PRODUCTION – SERIES I



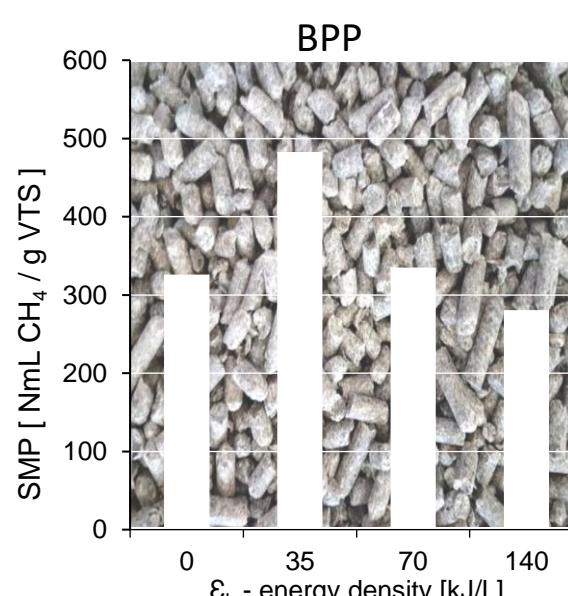
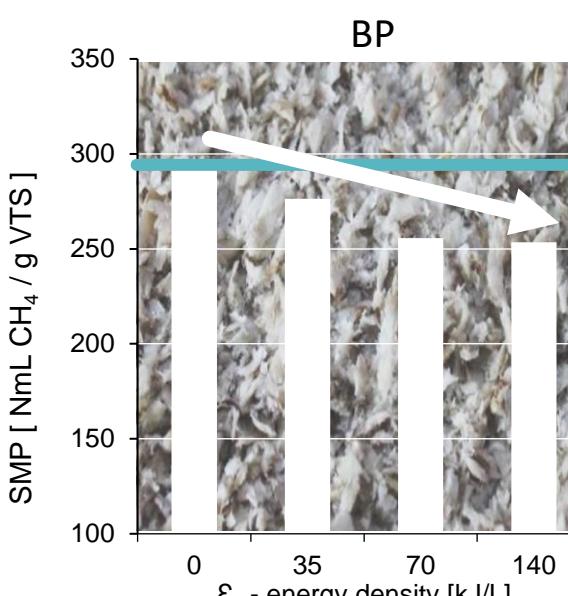
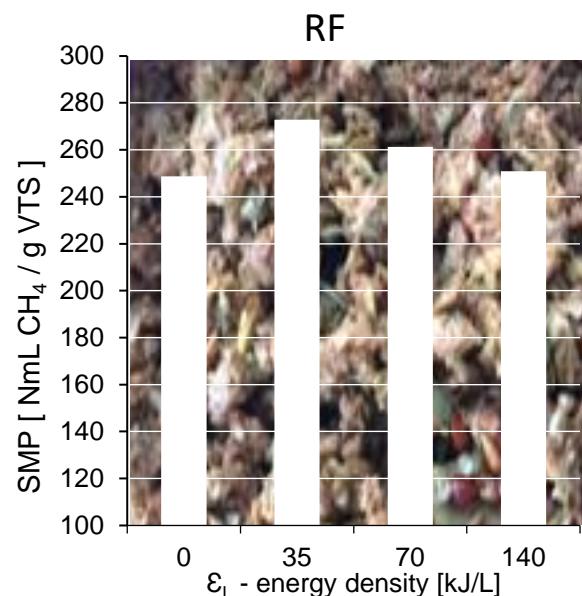
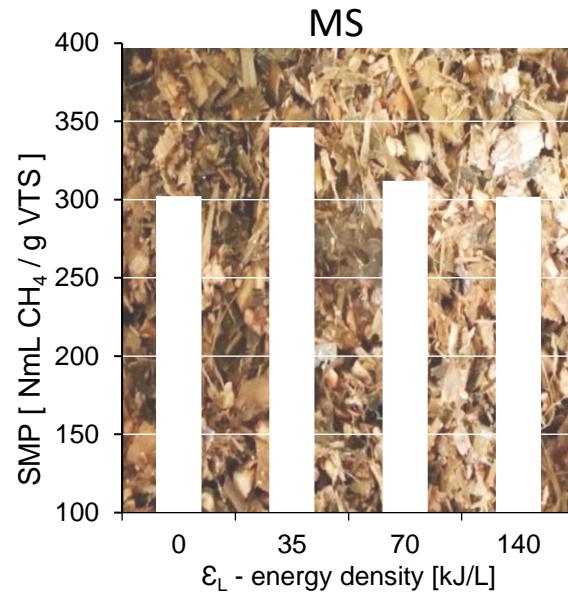
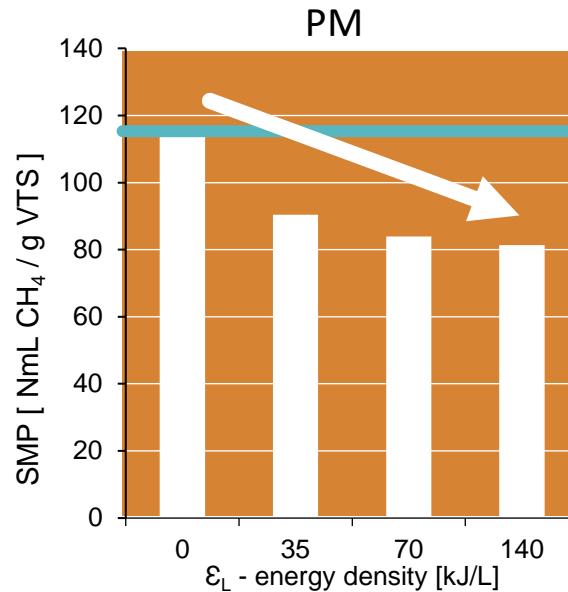
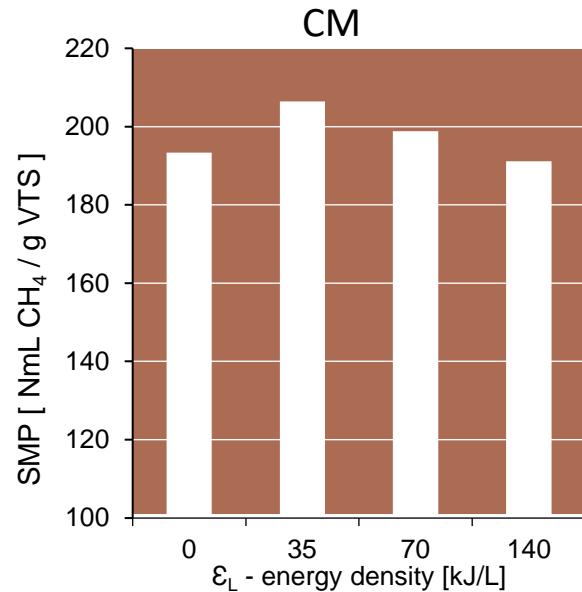
Biochemical methane potential (BMP) test

SPECIFIC METHANE PRODUCTION – SERIES I



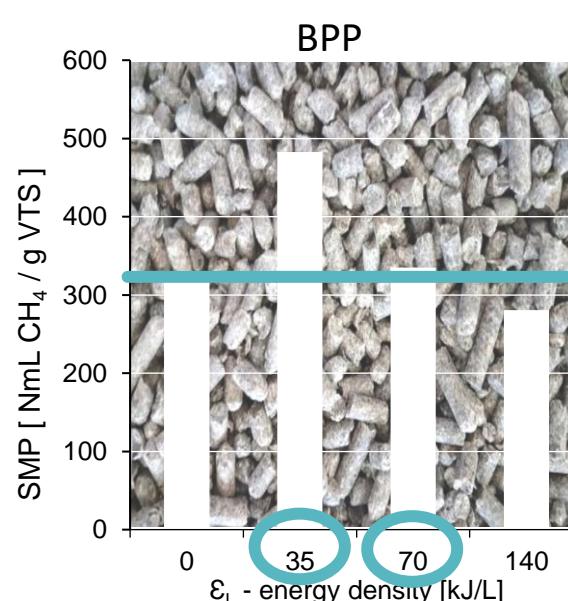
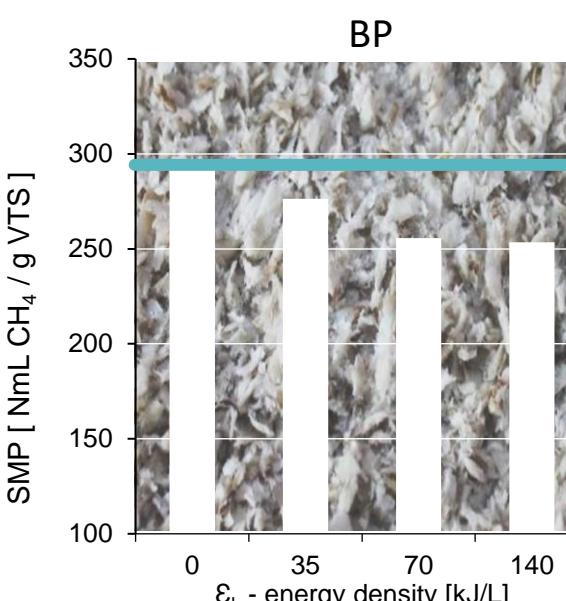
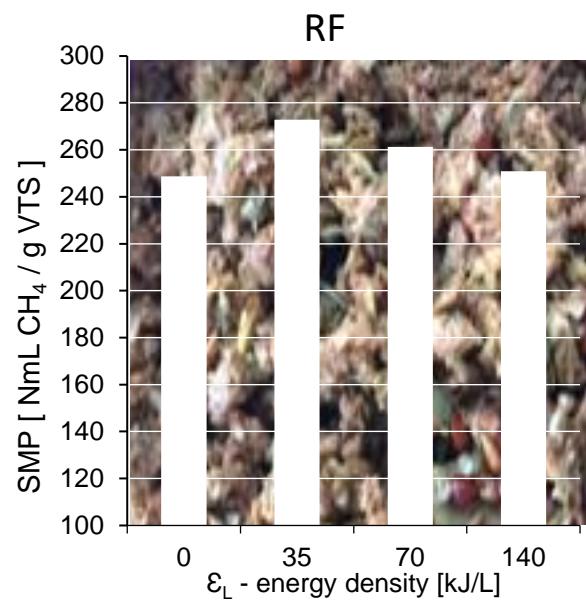
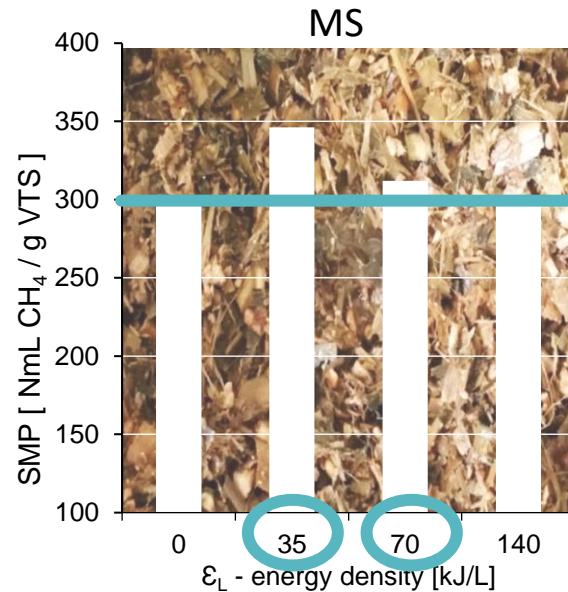
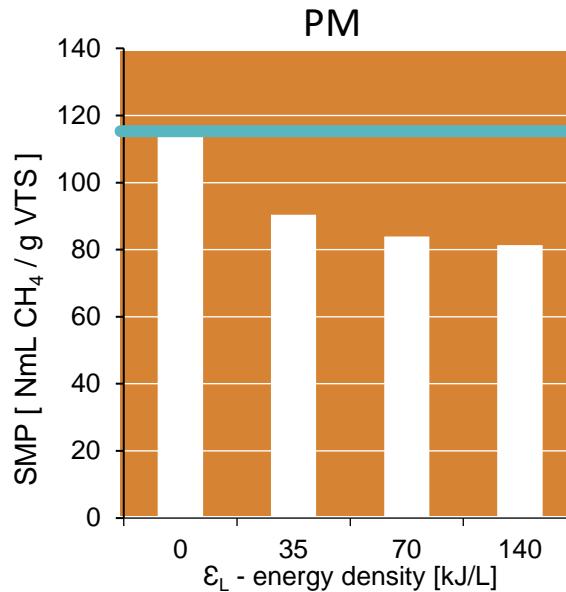
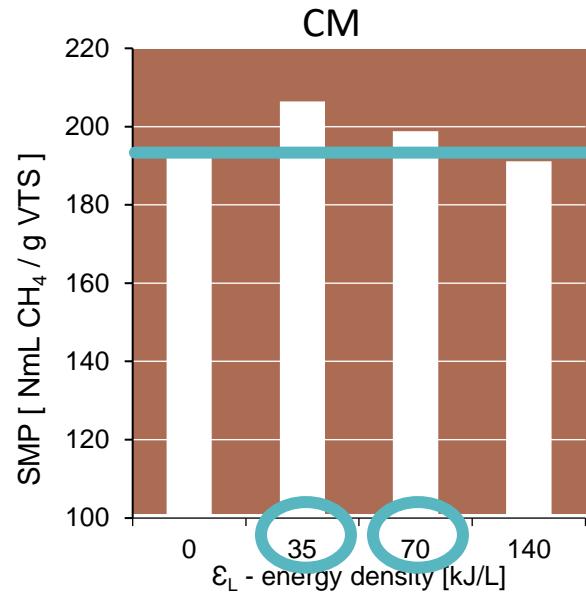
Biochemical methane potential (BMP) test

SPECIFIC METHANE PRODUCTION – SERIES I



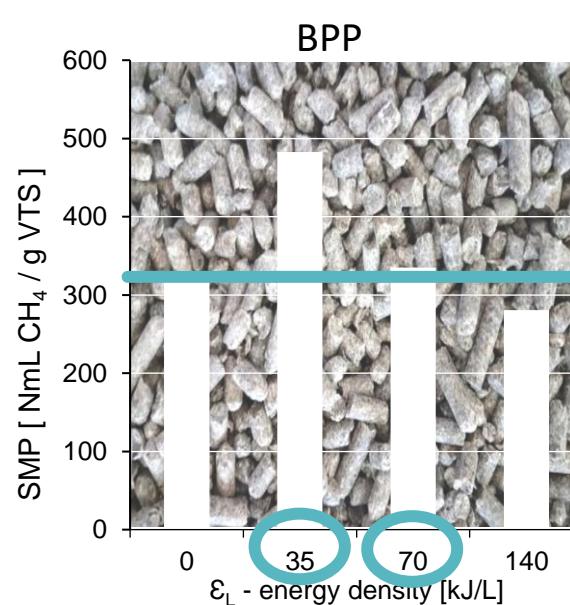
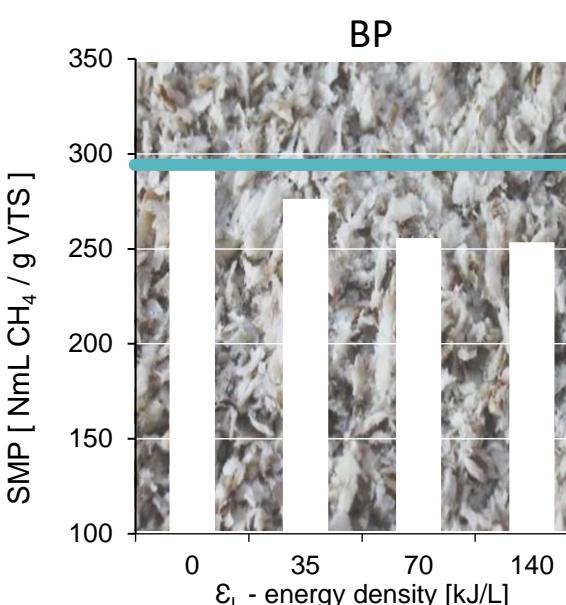
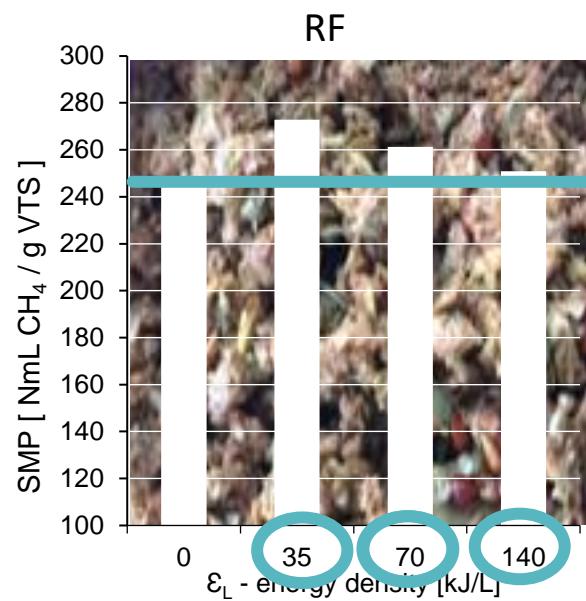
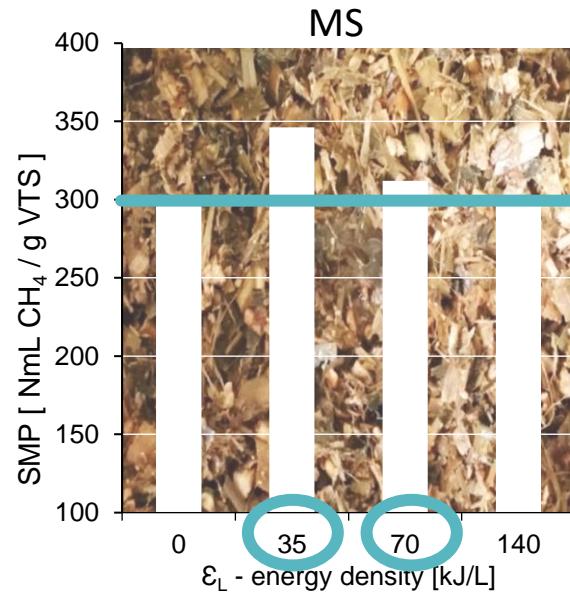
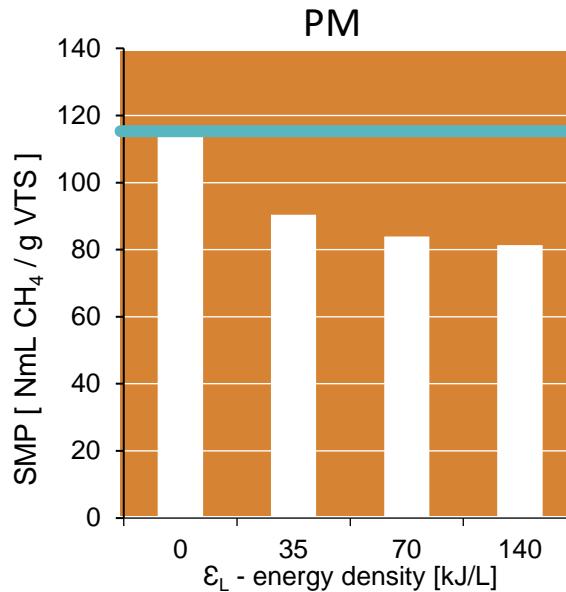
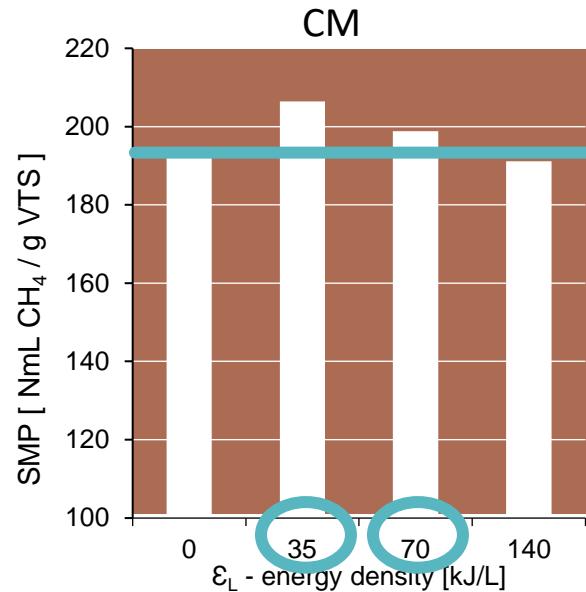
Biochemical methane potential (BMP) test

SPECIFIC METHANE PRODUCTION – SERIES I



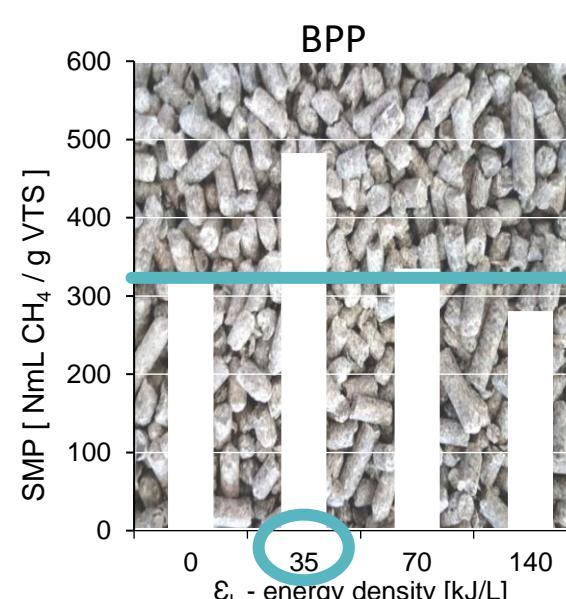
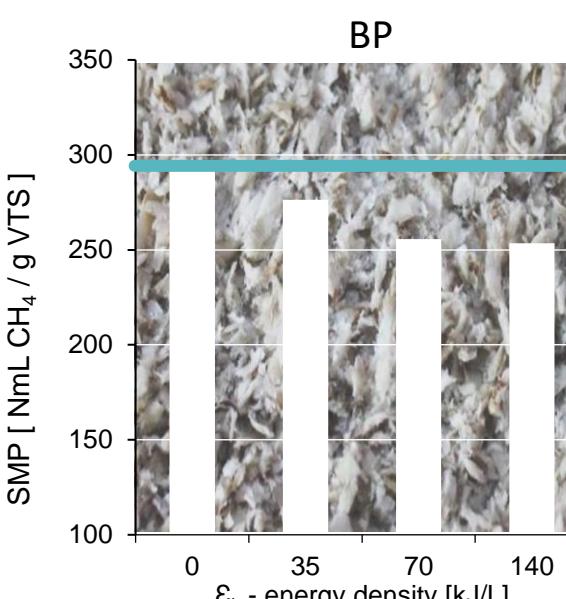
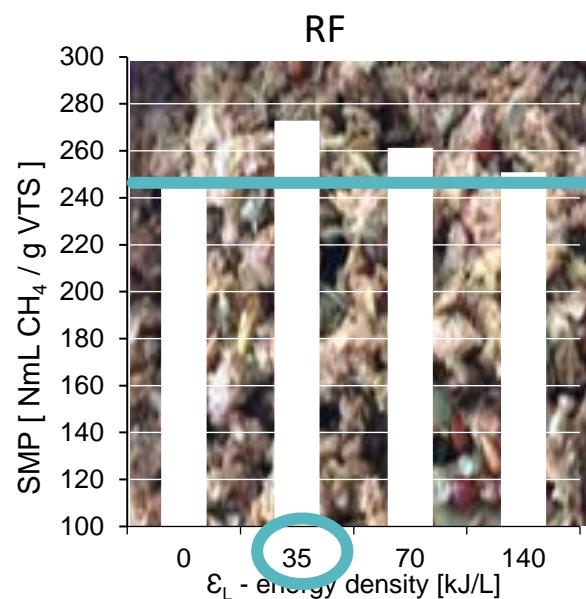
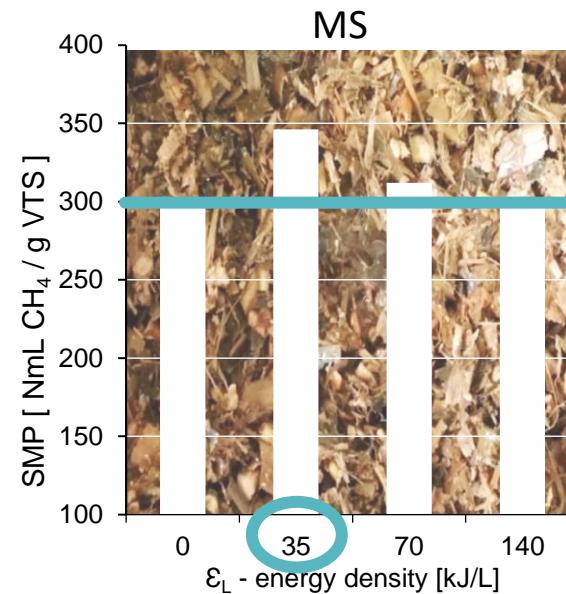
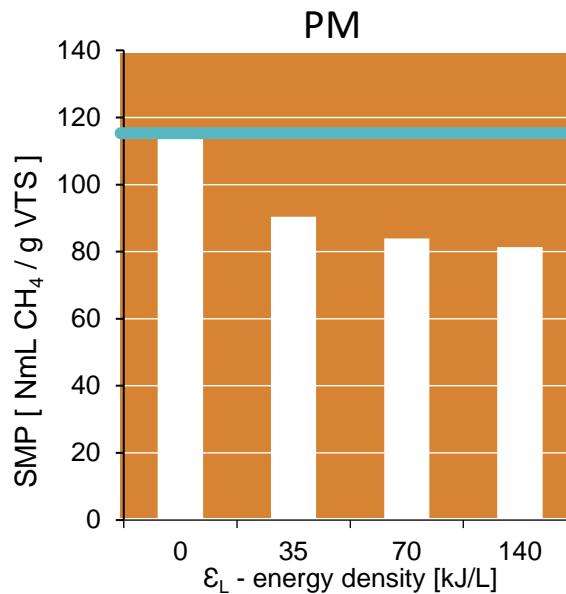
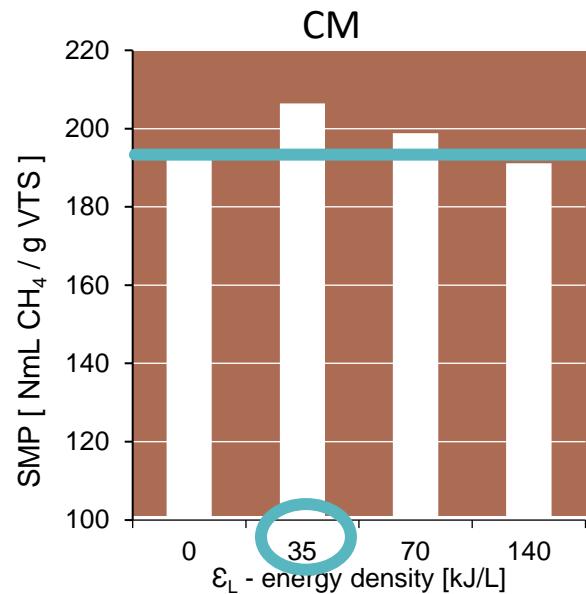
Biochemical methane potential (BMP) test

SPECIFIC METHANE PRODUCTION – SERIES I

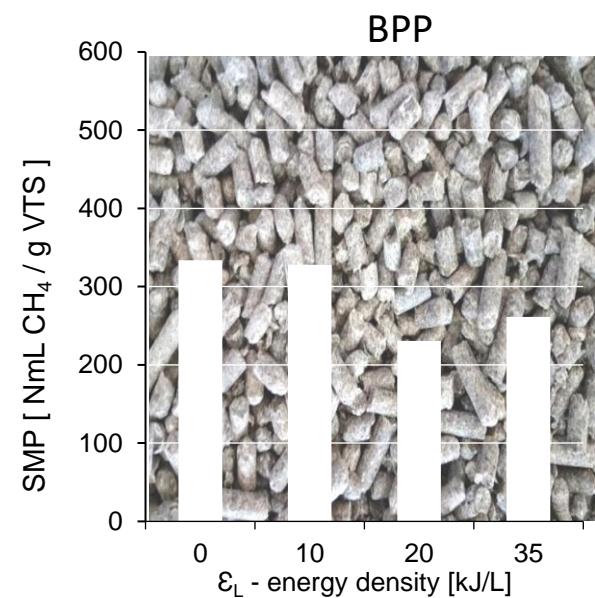
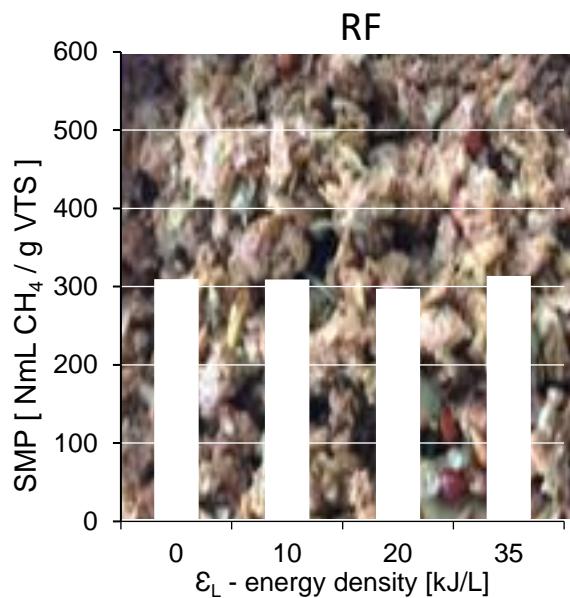
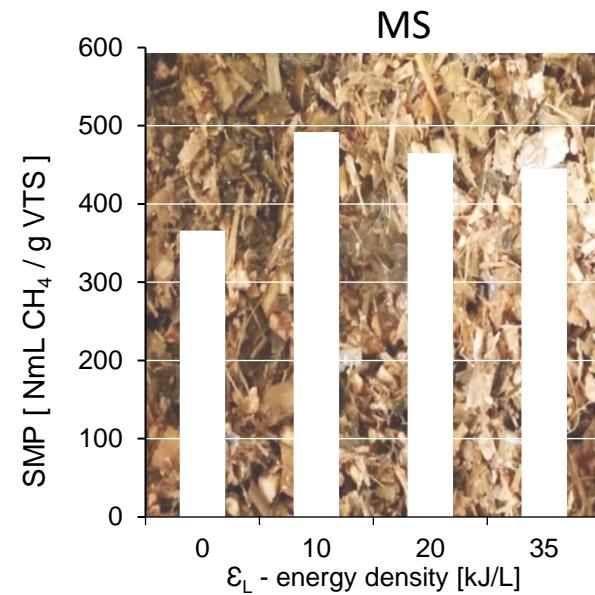
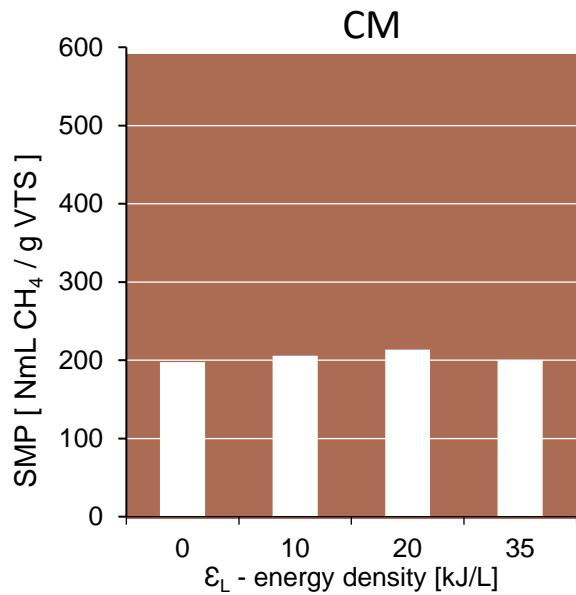


Biochemical methane potential (BMP) test

SPECIFIC METHANE PRODUCTION – SERIES I

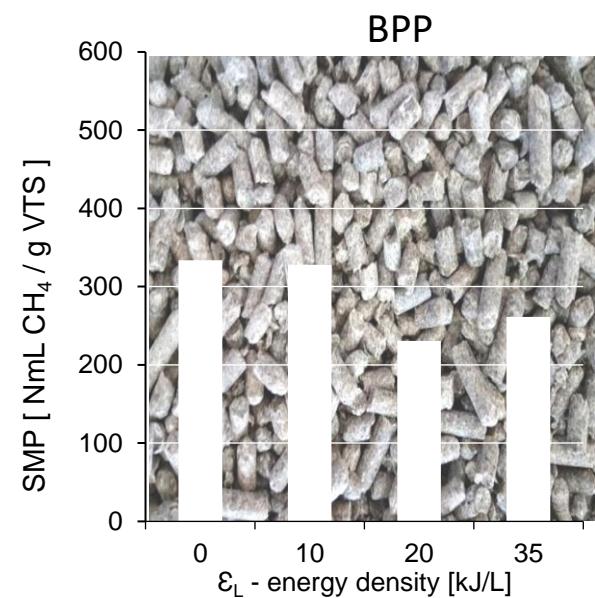
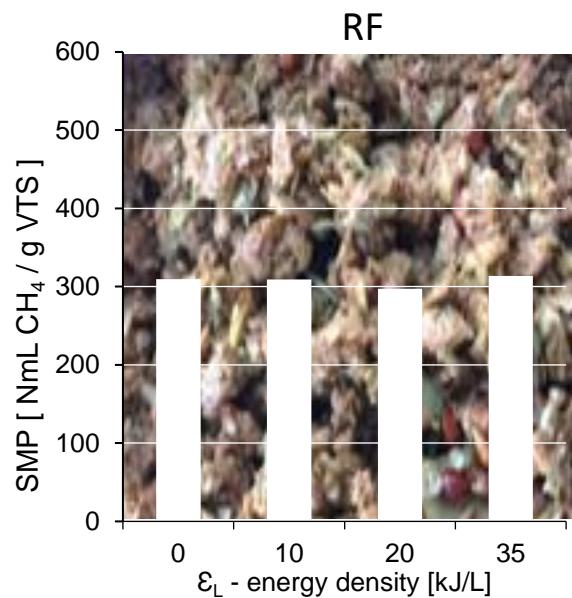
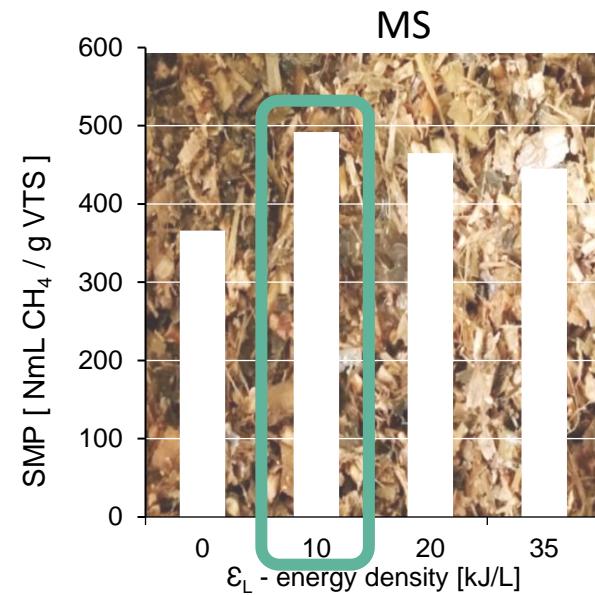
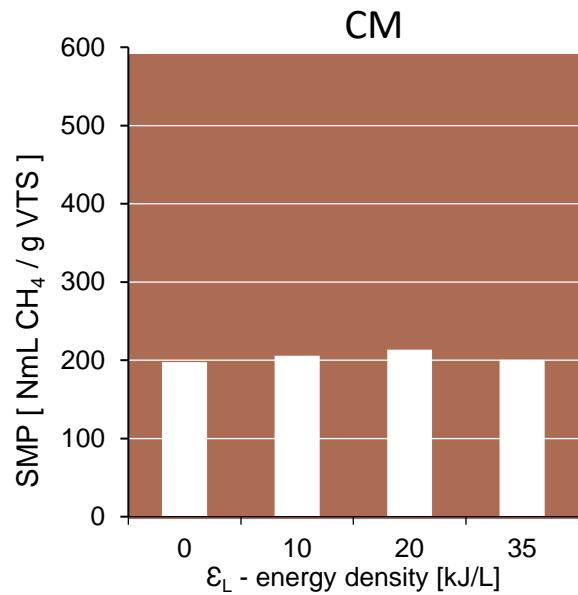


SPECIFIC METHANE PRODUCTION – SERIES 2

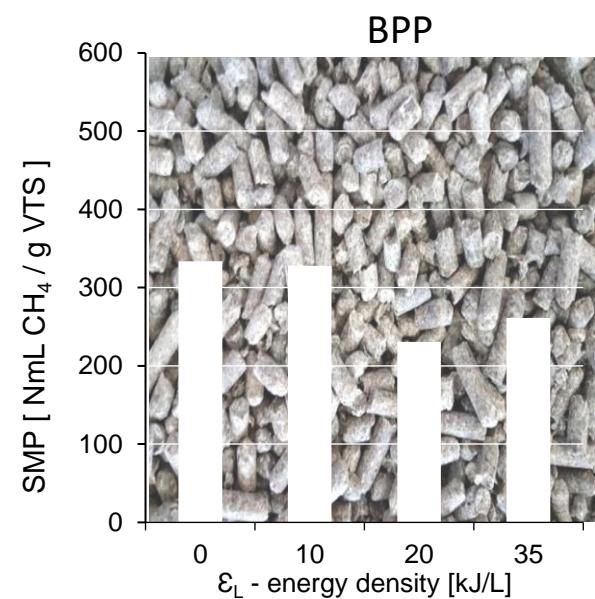
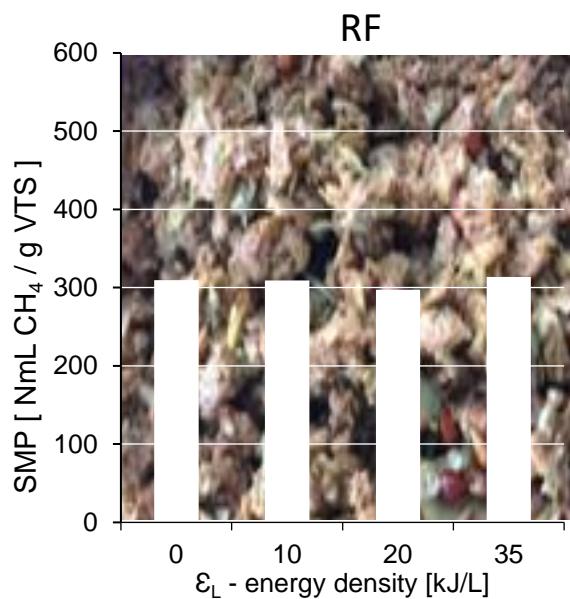
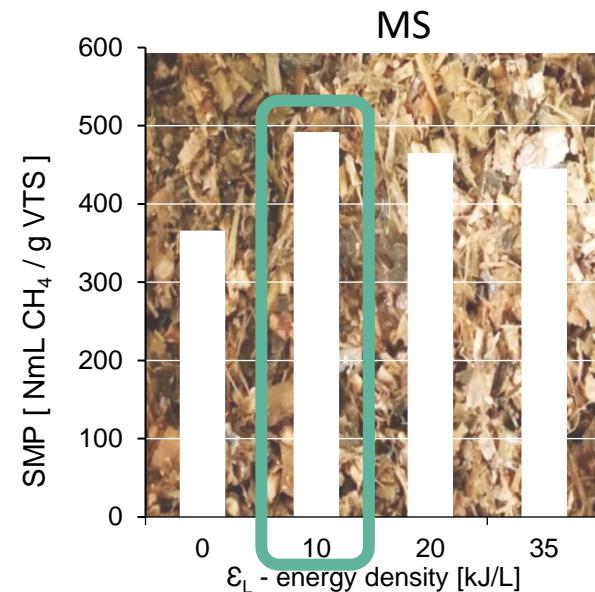
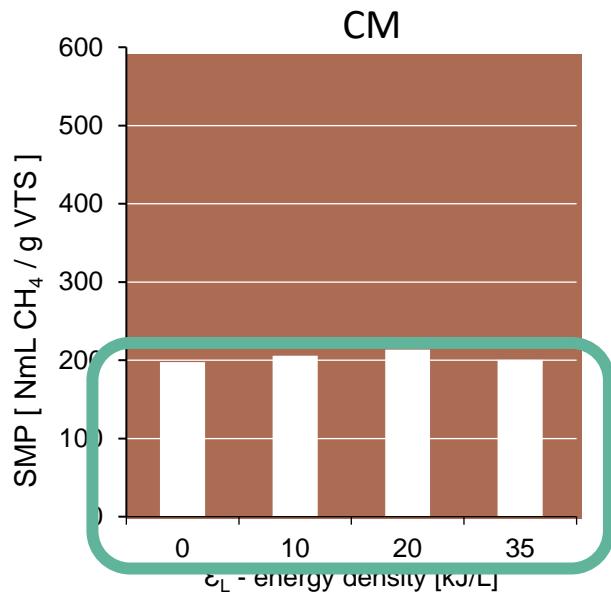


Biochemical methane potential (BMP) test

SPECIFIC METHANE PRODUCTION – SERIES 2

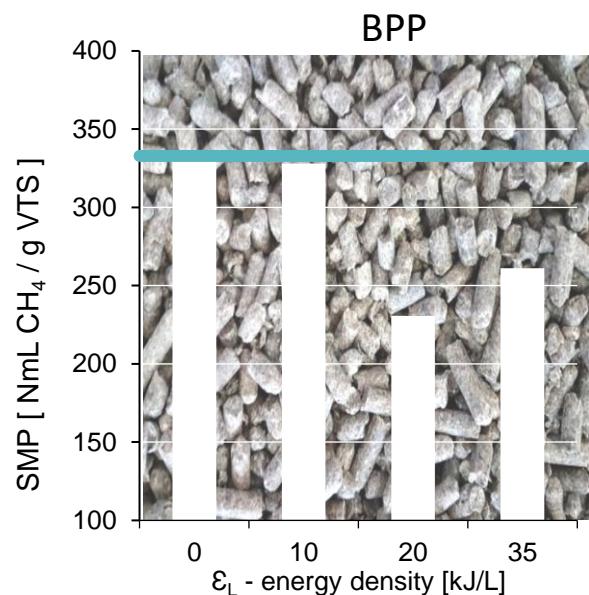
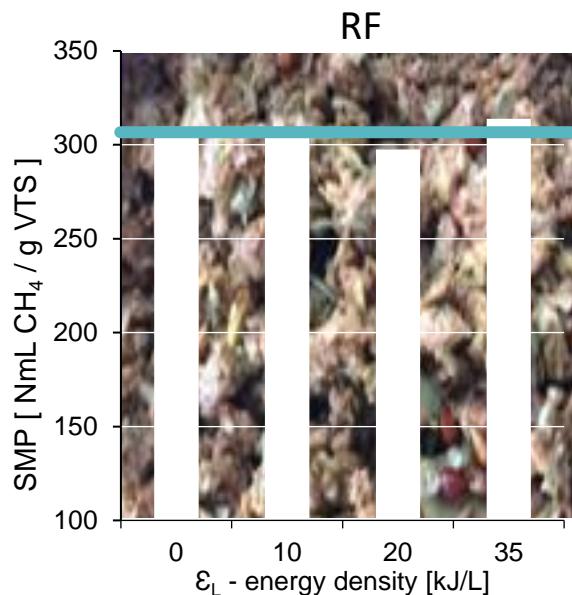
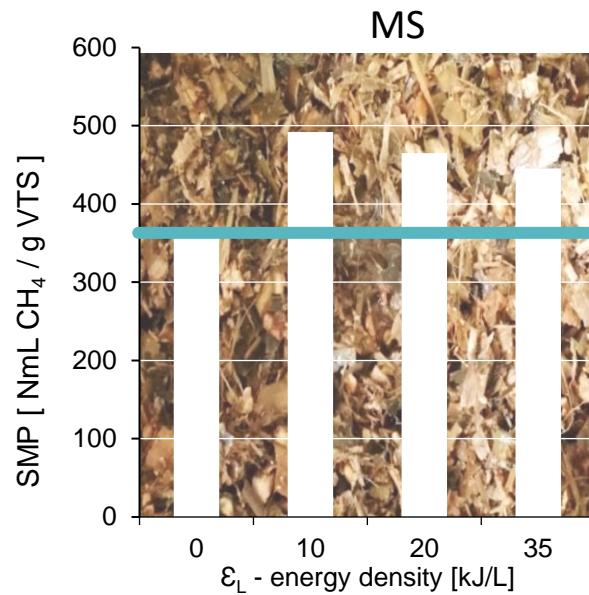
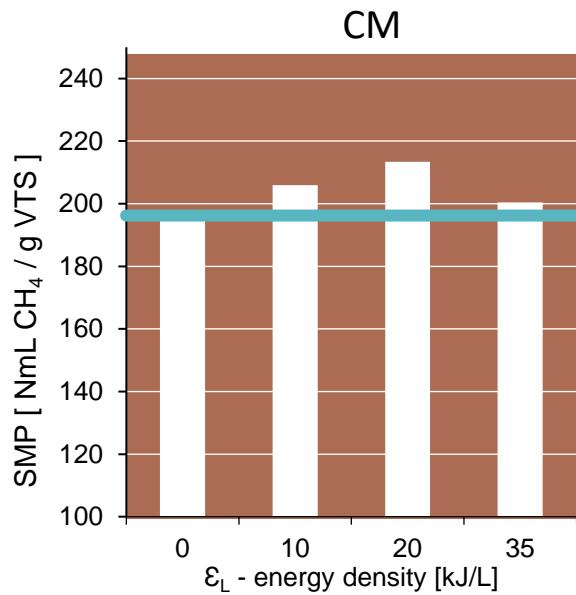


SPECIFIC METHANE PRODUCTION – SERIES 2



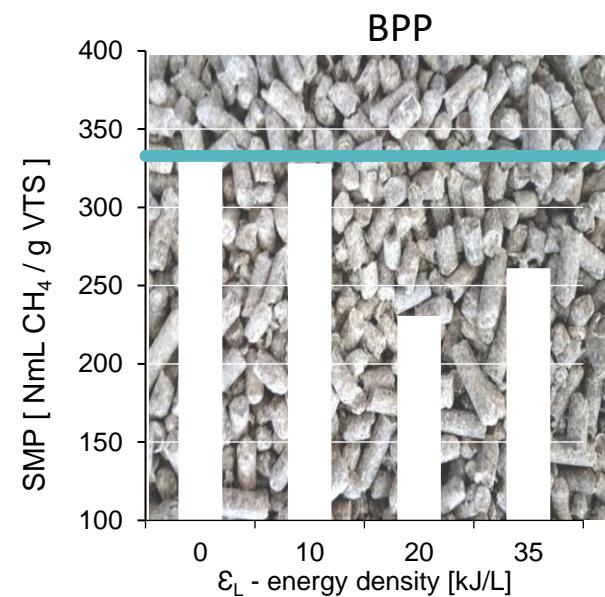
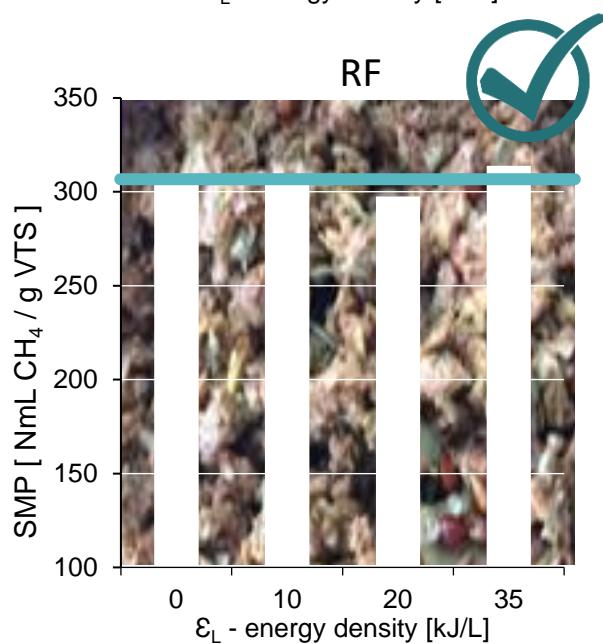
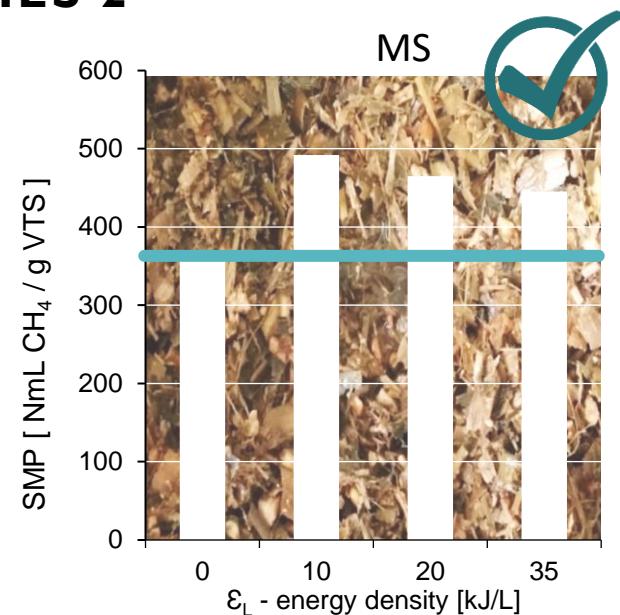
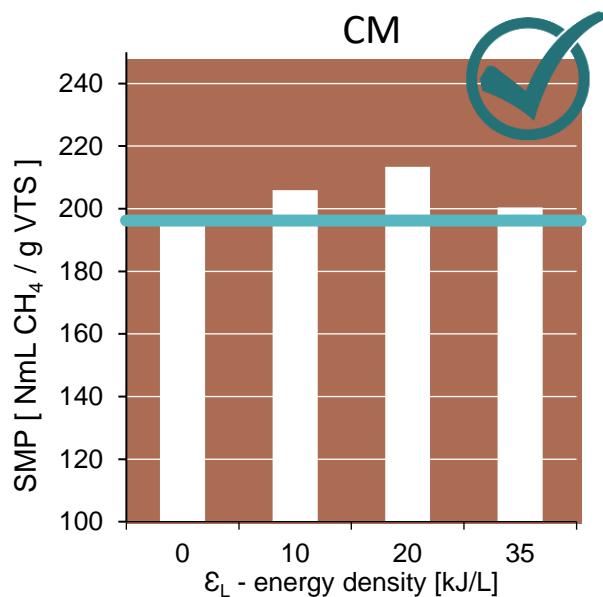
Biochemical methane potential (BMP) test

SPECIFIC METHANE PRODUCTION – SERIES 2



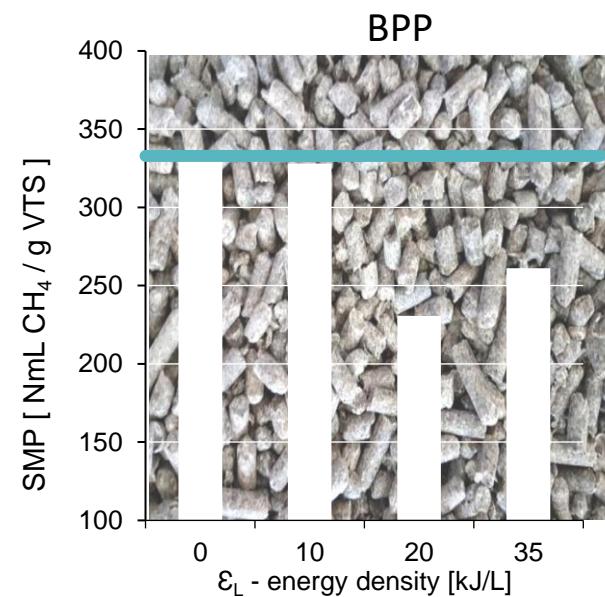
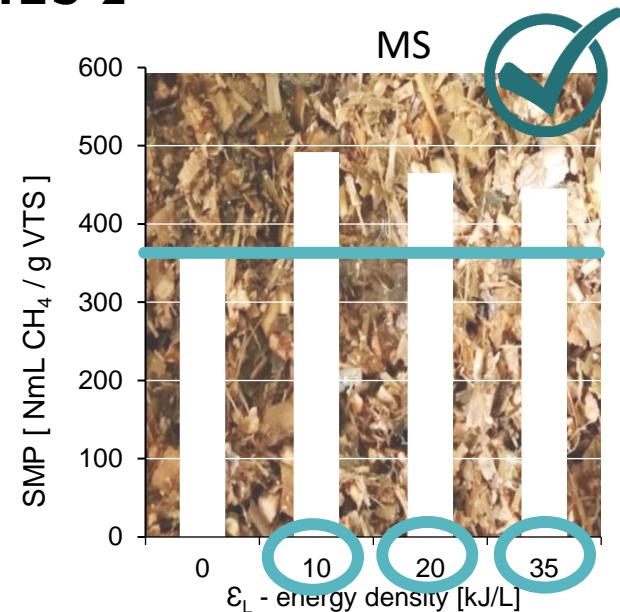
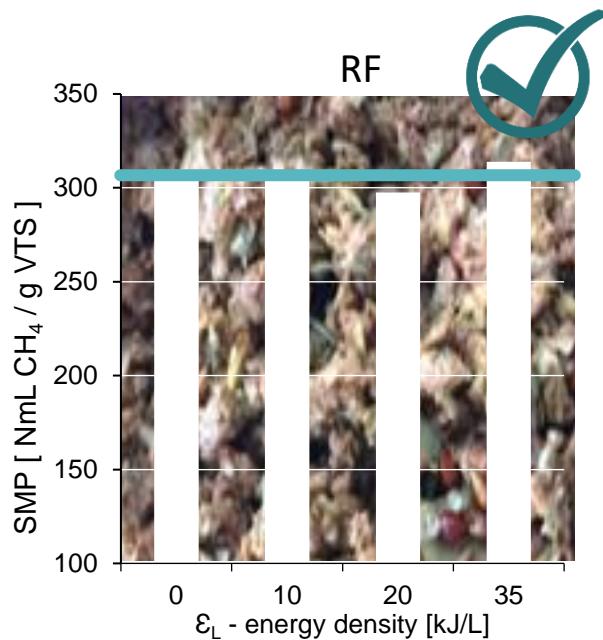
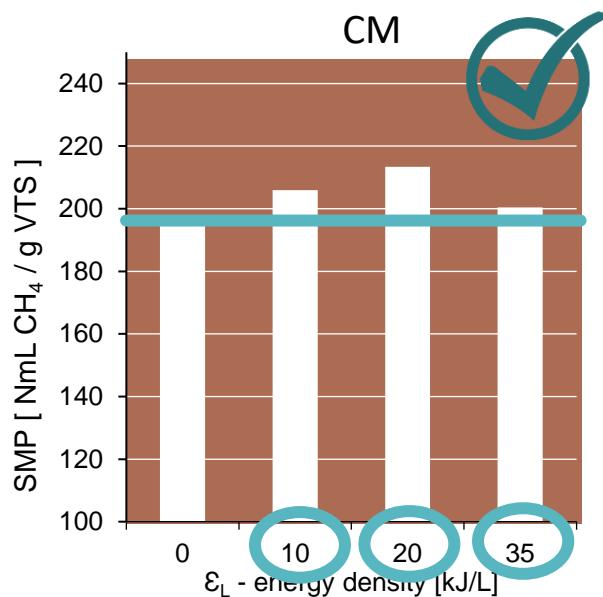
Biochemical methane potential (BMP) test

SPECIFIC METHANE PRODUCTION – SERIES 2



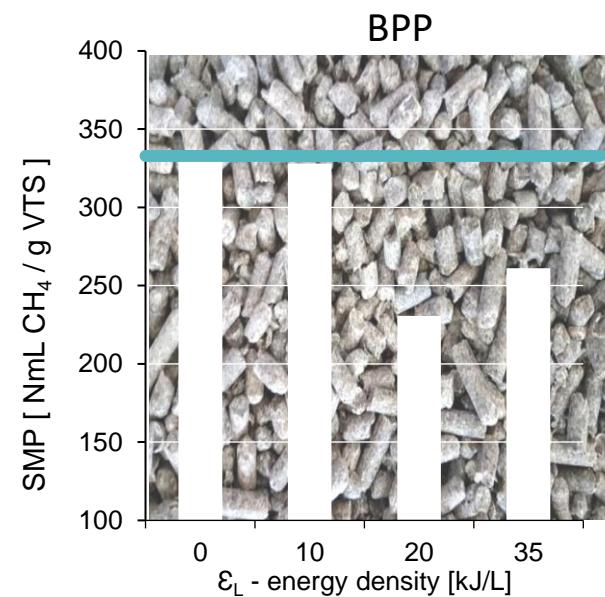
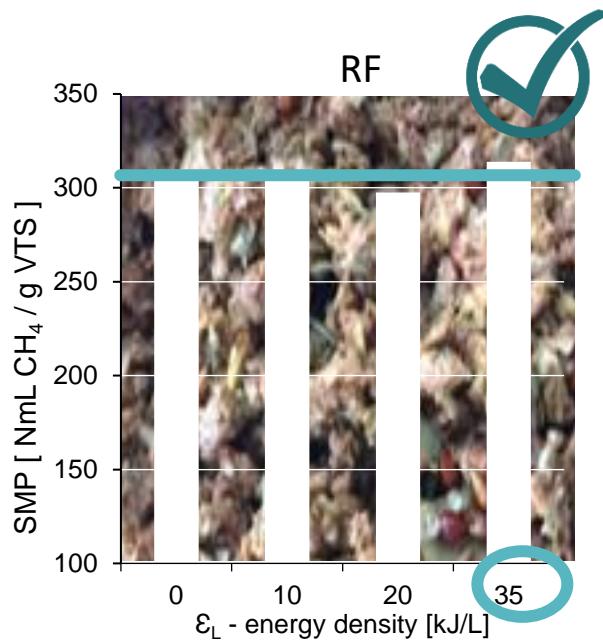
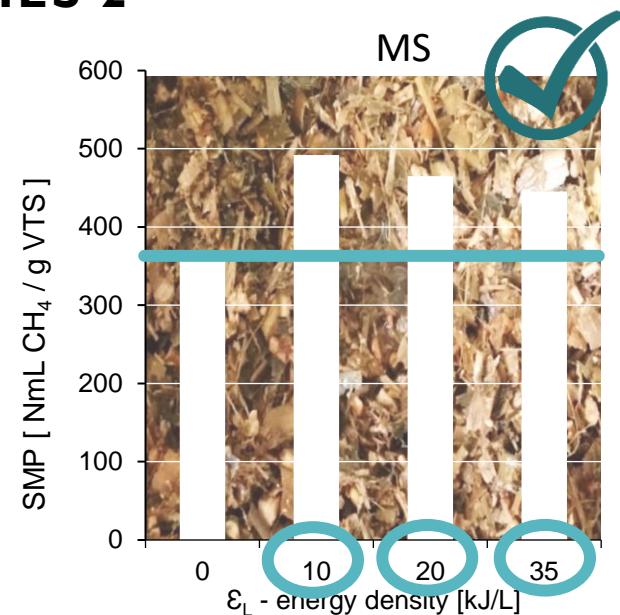
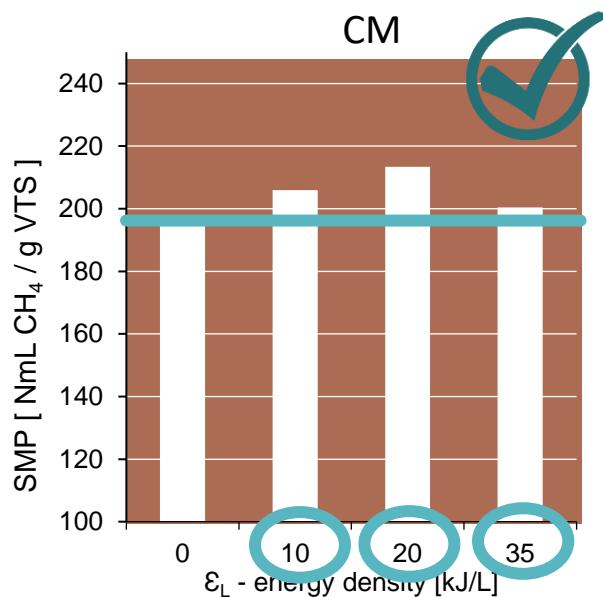
Biochemical methane potential (BMP) test

SPECIFIC METHANE PRODUCTION – SERIES 2

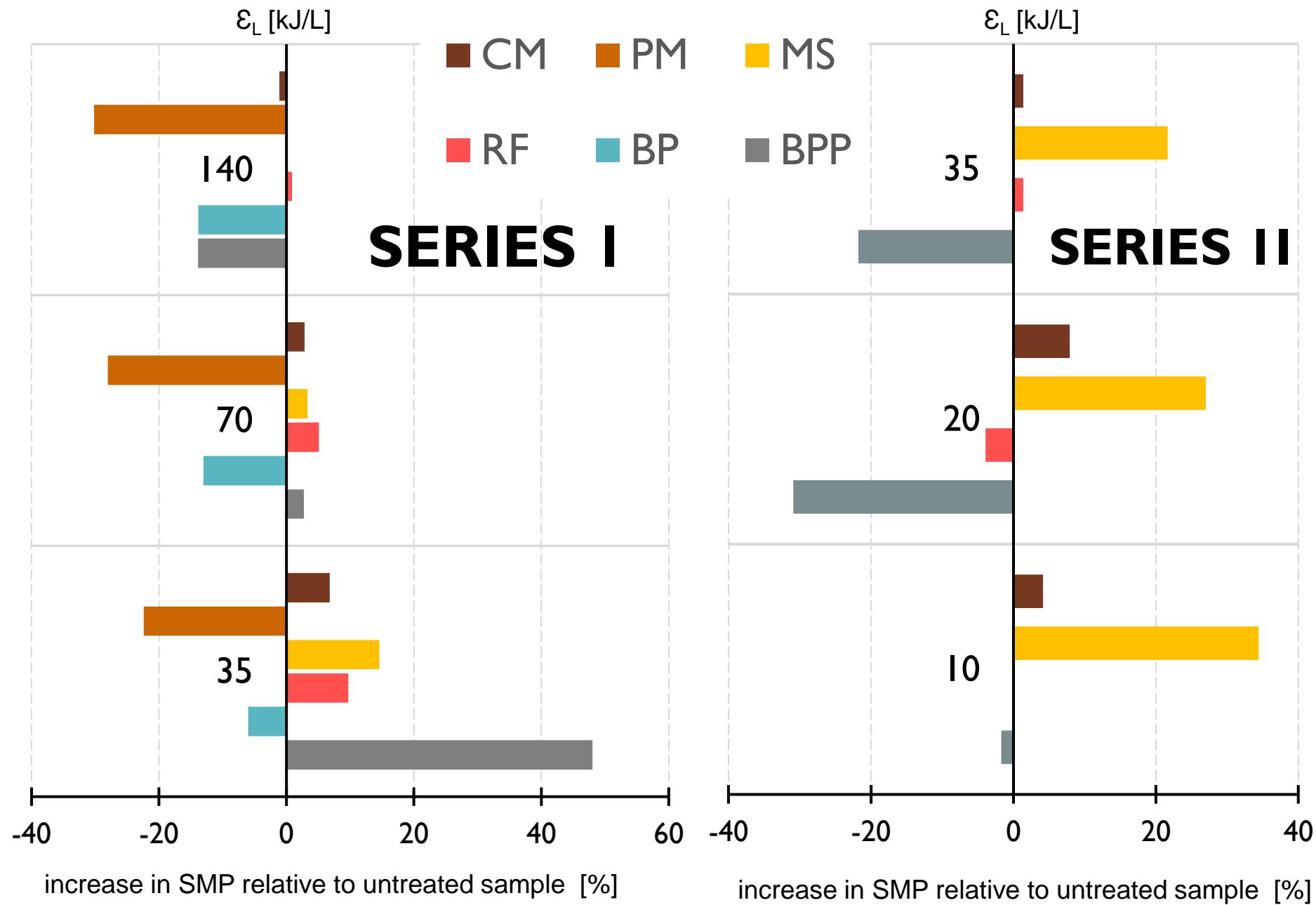


Biochemical methane potential (BMP) test

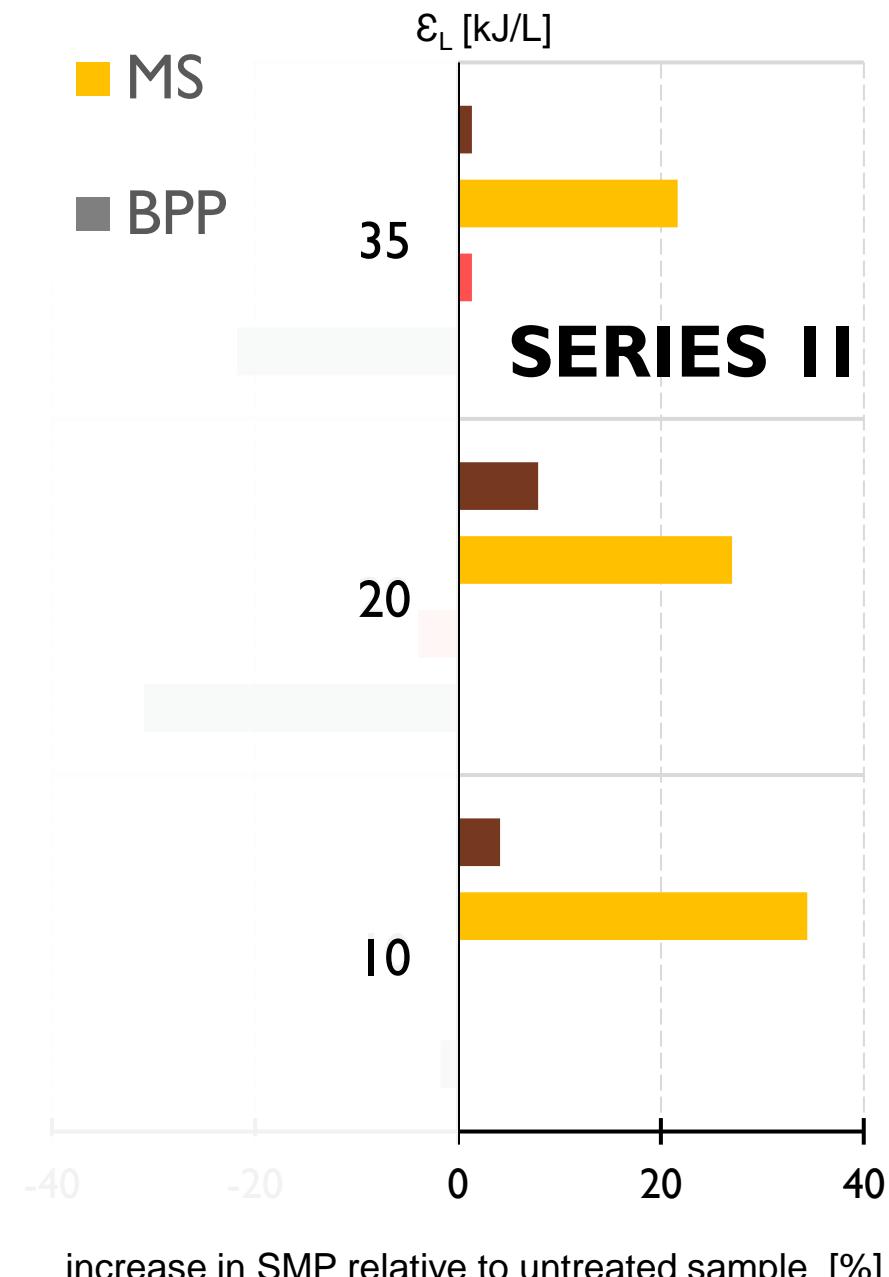
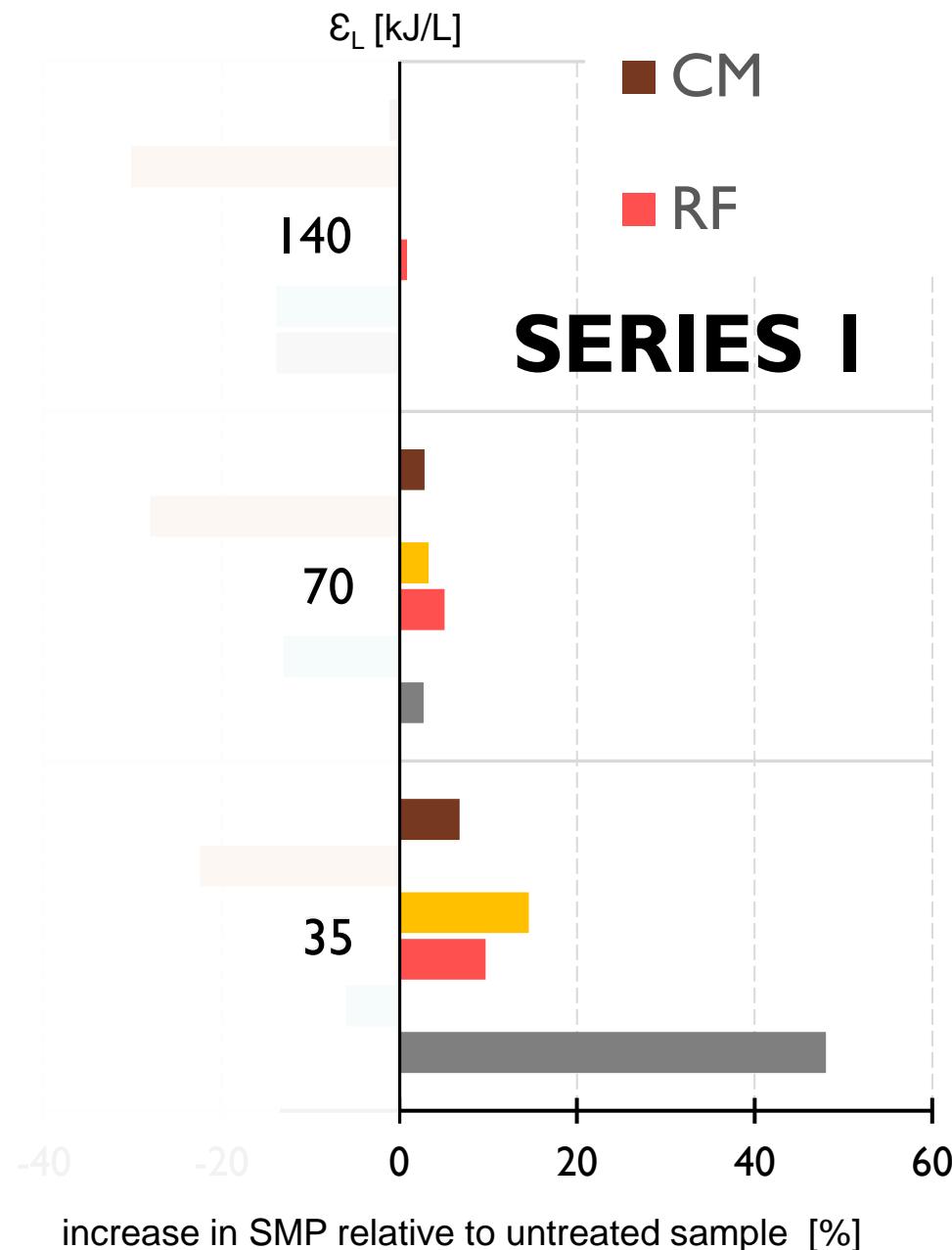
SPECIFIC METHANE PRODUCTION – SERIES 2



Effect of hydrodynamic disintegration on the Specific Methane Production (SMP)



Effect of hydrodynamic disintegration on the Specific Methane Production (SMP)



Energy balance

Parameter	unit	CM - Cow Manure								MS - Mazie Silage							
		Series 1				Series 2				Series 1				Series 2			
		0	35 kJ/L	70 kJ/L	140 kJ/L	0	10 kJ/L	20 kJ/L	35 kJ/L	0	35 kJ/L	70 kJ/L	140 kJ/L	0	10 kJ/L	20 kJ/L	35 kJ/L
Methane energy content ¹	Wh	3,86	4,10	3,95	3,79	3,95	4,11	4,25	3,99	3,12	3,45	3,11	3,00	7,29	9,81	9,27	8,87
Electricity ²	Wh	1,54	1,64	1,58	1,51	1,58	1,64	1,70	1,60	1,25	1,38	1,25	1,20	2,92	3,92	3,71	3,55
Extra electricity ³	Wh		0,10	0,04	-0,03		0,06	0,12	0,02		0,13	0,00	-0,04		1,01	0,79	0,63
Energy applied for HD	Wh		0,26	0,52	1,04		0,09	0,18	0,32		0,23	0,42			0,17	0,31	0,58
Net energy production	Wh		-0,16	-0,48			-0,03	-0,05	-0,30		-0,10	-0,42			0,84	0,48	0,05
Relative energy profit	%														599	253	108

Parameter	unit	RF - Remains of Fruits								BPP - Beetroot Pulp in the form of Pellets							
		Series 1				Series 2				Series 1				Series 2			
		0	35 kJ/L	70 kJ/L	140 kJ/L	0	10 kJ/L	20 kJ/L	35 kJ/L	0	35 kJ/L	70 kJ/L	140 kJ/L	0	10 kJ/L	20 kJ/L	35 kJ/L
Methane energy content ¹	Wh	2,48	2,70	2,63	2,52	6,12	6,17	5,92	6,25	6,51	9,61	6,65	5,60	6,65	6,66	4,60	5,21
Electricity ²	Wh	0,99	1,08	1,05	1,01	2,45	2,47	2,37	2,50	2,60	3,84	2,66	2,24	2,66	2,66	1,84	2,08
Extra electricity ³	Wh		0,09	0,06	0,02		0,02	-0,08	0,05		1,24	0,06	-0,36		0,00	-0,82	-0,58
Energy applied for HD	Wh		0,20	0,39	0,78		0,10		0,38		0,41	0,82					
Net energy production	Wh		-0,11	-0,33	-0,77		-0,09		-0,33		0,83	-0,76					
Relative energy profit	%									303							

¹Methane energy content calculated by assuming methane calorific value equal to 36 MJ/m³;

²Electricity calculated by assuming electrical efficiency of engine equal to 40%;

³Extra electricity = electricity dez.—electricity untreated, (Wh): Electricity dez., amount of electricity produced in a disintegrated sample at a predefined energy density level (Wh); Electricity untreated, amount of electricity produced in an untreated sample (Wh).

Energy balance

Parameter	unit	CM - Cow Manure								MS - Mazie Silage							
		Series 1				Series 2				Series 1				Series 2			
		0	35 kJ/L	70 kJ/L	140 kJ/L	0	10 kJ/L	20 kJ/L	35 kJ/L	0	35 kJ/L	70 kJ/L	140 kJ/L	0	10 kJ/L	20 kJ/L	35 kJ/L
Methane energy content ¹	Wh	3,86	4,10	3,95	3,79	3,95	4,11	4,25	3,99	3,12	3,45	3,11	3,00	7,29	9,81	9,27	8,87
Electricity ²	Wh	1,54	1,64	1,58	1,51	1,58	1,64	1,70	1,60	1,25	1,38	1,25	1,20	2,92	3,92	3,71	3,55
Extra electricity ³	Wh		0,10	0,04	-0,03		0,06	0,12	0,02		0,13	0,00	-0,04		1,01	0,79	0,63
Energy applied for HD	Wh		0,26	0,52	1,04		0,09	0,18	0,32		0,23	0,42			0,17	0,31	0,58
Net energy production	Wh		-0,16	-0,48			-0,03	-0,05	-0,30		-0,10	-0,42			0,84	0,48	0,05
Relative energy profit	%														599	253	108

Parameter	unit	RF - Remains of Fruits								BPP - Beetroot Pulp in the form of Pellets							
		Series 1				Series 2				Series 1				Series 2			
		0	35 kJ/L	70 kJ/L	140 kJ/L	0	10 kJ/L	20 kJ/L	35 kJ/L	0	35 kJ/L	70 kJ/L	140 kJ/L	0	10 kJ/L	20 kJ/L	35 kJ/L
Methane energy content ¹	Wh	2,48	2,70	2,63	2,52	6,12	6,17	5,92	6,25	6,51	9,61	6,65	5,60	6,65	6,66	4,60	5,21
Electricity ²	Wh	0,99	1,08	1,05	1,01	2,45	2,47	2,37	2,50	2,60	3,84	2,66	2,24	2,66	2,66	1,84	2,08
Extra electricity ³	Wh		0,09	0,06	0,02		0,02	-0,08	0,05		1,24	0,06	-0,36		0,00	-0,82	-0,58
Energy applied for HD	Wh		0,20	0,39	0,78		0,10		0,38		0,41	0,82					
Net energy production	Wh		-0,11	-0,33	-0,77		-0,09		-0,33		0,83	-0,76					
Relative energy profit	%									303							

¹Methane energy content calculated by assuming methane calorific value equal to 36 MJ/m³;

²Electricity calculated by assuming electrical efficiency of engine equal to 40%;

³Extra electricity = electricity dez.—electricity untreated, (Wh): Electricity dez., amount of electricity produced in a disintegrated sample at a predefined energy density level (Wh); Electricity untreated, amount of electricity produced in an untreated sample (Wh).

Energy balance

Parameter	unit	CM - Cow Manure								MS - Mazie Silage							
		Series 1				Series 2				Series 1				Series 2			
		0	35 kJ/L	70 kJ/L	140 kJ/L	0	10 kJ/L	20 kJ/L	35 kJ/L	0	35 kJ/L	70 kJ/L	140 kJ/L	0	10 kJ/L	20 kJ/L	35 kJ/L
Methane energy content ¹	Wh	3,86	4,10	3,95	3,79	3,95	4,11	4,25	3,99	3,12	3,45	3,11	3,00	7,29	9,81	9,27	8,87
Electricity ²	Wh	1,54	1,64	1,58	1,51	1,58	1,64	1,70	1,60	1,25	1,38	1,25	1,20	2,92	3,92	3,71	3,55
Extra electricity ³	Wh		0,10	0,04	-0,03		0,06	0,12	0,02		0,13	0,00	-0,04		1,01	0,79	0,63
Energy applied for HD	Wh		0,26	0,52	1,04		0,09	0,18	0,32		0,23	0,42			0,17	0,31	0,58
Net energy production	Wh		-0,16	-0,48			-0,03	-0,05	-0,30		-0,10	-0,42			0,84	0,48	0,05
Relative energy profit	%														599	253	108

Parameter	unit	RF - Remains of Fruits								BPP - Beetroot Pulp in the form of Pellets							
		Series 1				Series 2				Series 1				Series 2			
		0	35 kJ/L	70 kJ/L	140 kJ/L	0	10 kJ/L	20 kJ/L	35 kJ/L	0	35 kJ/L	70 kJ/L	140 kJ/L	0	10 kJ/L	20 kJ/L	35 kJ/L
Methane energy content ¹	Wh	2,48	2,70	2,63	2,52	6,12	6,17	5,92	6,25	6,51	9,61	6,65	5,60	6,65	6,66	4,60	5,21
Electricity ²	Wh	0,99	1,08	1,05	1,01	2,45	2,47	2,37	2,50	2,60	3,84	2,66	2,24	2,66	2,66	1,84	2,08
Extra electricity ³	Wh		0,09	0,06	0,02		0,02	-0,08	0,05		1,24	0,06	-0,36		0,00	-0,82	-0,58
Energy applied for HD	Wh		0,20	0,39	0,78		0,10		0,38		0,41	0,82					
Net energy production	Wh		-0,11	-0,33	-0,77		-0,09		-0,33		0,83	-0,76					
Relative energy profit	%										303						

¹Methane energy content calculated by assuming methane calorific value equal to 36 MJ/m³;

²Electricity calculated by assuming electrical efficiency of engine equal to 40%;

³Extra electricity = electricity dez.—electricity untreated, (Wh): Electricity dez., amount of electricity produced in a disintegrated sample at a predefined energy density level (Wh); Electricity untreated, amount of electricity produced in an untreated sample (Wh).

Energy balance

Parameter	unit	CM - Cow Manure								MS - Mazie Silage							
		Series 1				Series 2				Series 1				Series 2			
		0	35 kJ/L	70 kJ/L	140 kJ/L	0	10 kJ/L	20 kJ/L	35 kJ/L	0	35 kJ/L	70 kJ/L	140 kJ/L	0	10 kJ/L	20 kJ/L	35 kJ/L
Methane energy content ¹	Wh	3,86	4,10	3,95	3,79	3,95	4,11	4,25	3,99	3,12	3,45	3,11	3,00	7,29	9,81	9,27	8,87
Electricity ²	Wh	1,54	1,64	1,58	1,51	1,58	1,64	1,70	1,60	1,25	1,38	1,25	1,20	2,92	3,92	3,71	3,55
Extra electricity ³	Wh		0,10	0,04	-0,03		0,06	0,12	0,02		0,13	0,00	-0,04		1,01	0,79	0,63
Energy applied for HD	Wh		0,26	0,52	1,04		0,09	0,18	0,32		0,23	0,42			0,17	0,31	0,58
Net energy production	Wh		-0,16	-0,48			-0,03	-0,05	-0,30		-0,10	-0,42			0,84	0,48	0,05
Relative energy profit	%														599	253	108

Parameter	unit	RF - Remains of Fruits								BPP - Beetroot Pulp in the form of Pellets							
		Series 1				Series 2				Series 1				Series 2			
		0	35 kJ/L	70 kJ/L	140 kJ/L	0	10 kJ/L	20 kJ/L	35 kJ/L	0	35 kJ/L	70 kJ/L	140 kJ/L	0	10 kJ/L	20 kJ/L	35 kJ/L
Methane energy content ¹	Wh	2,48	2,70	2,63	2,52	6,12	6,17	5,92	6,25	6,51	9,61	6,65	5,60	6,65	6,66	4,60	5,21
Electricity ²	Wh	0,99	1,08	1,05	1,01	2,45	2,47	2,37	2,50	2,60	3,84	2,66	2,24	2,66	2,66	1,84	2,08
Extra electricity ³	Wh		0,09	0,06	0,02		0,02	-0,08	0,05		1,24	0,06	-0,36		0,00	-0,82	-0,58
Energy applied for HD	Wh		0,20	0,39	0,78		0,10		0,38		0,41	0,82					
Net energy production	Wh		-0,11	-0,33	-0,77		-0,09		-0,33		0,83	-0,76					
Relative energy profit	%									303							

¹Methane energy content calculated by assuming methane calorific value equal to 36 MJ/m³;

²Electricity calculated by assuming electrical efficiency of engine equal to 40%;

³Extra electricity = electricity dez.—electricity untreated, (Wh): Electricity dez., amount of electricity produced in a disintegrated sample at a predefined energy density level (Wh); Electricity untreated, amount of electricity produced in an untreated sample (Wh).

CONCLUSIONS

Hydrodynamic disintegration as pre-treatment of substrates subject to the anaerobic digestion process allows for increasing the amount of produced methane while obtaining a positive energy balance.

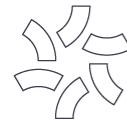
Implementation works should be preceded with tests aimed at the selection of:

- substrate/substrates subject to pre-treatment
 - ~~cow manure~~ pig manure **maize silage** remains of fruits
~~beetroot pulp~~ **beetroot pulp in the form of pellets**
- parameters of the disintegration process (including the amount of energy supplied in the process)

10 kJ/L 20 kJ/L 35 kJ/L 70 kJ/L 140 kJ/L



Warsaw University of Technology



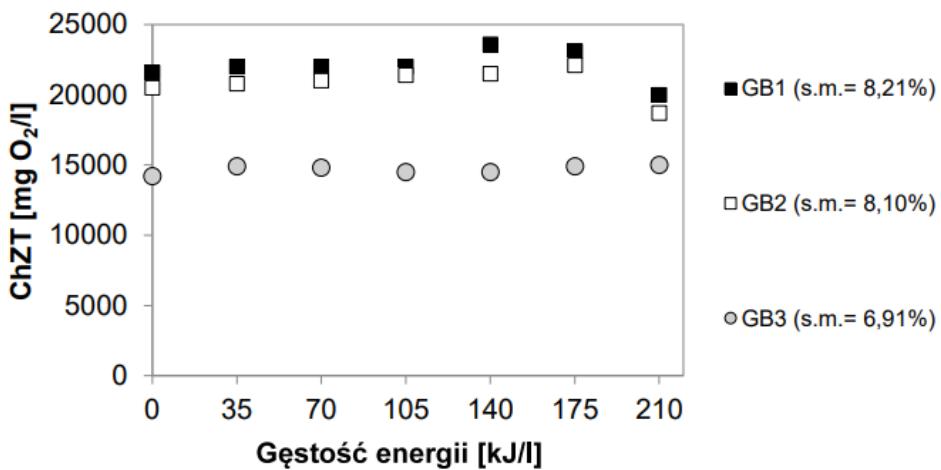
**Faculty of Building
Services, Hydro and
Environmental Engineering**

WARSAW UNIVERSITY OF TECHNOLOGY

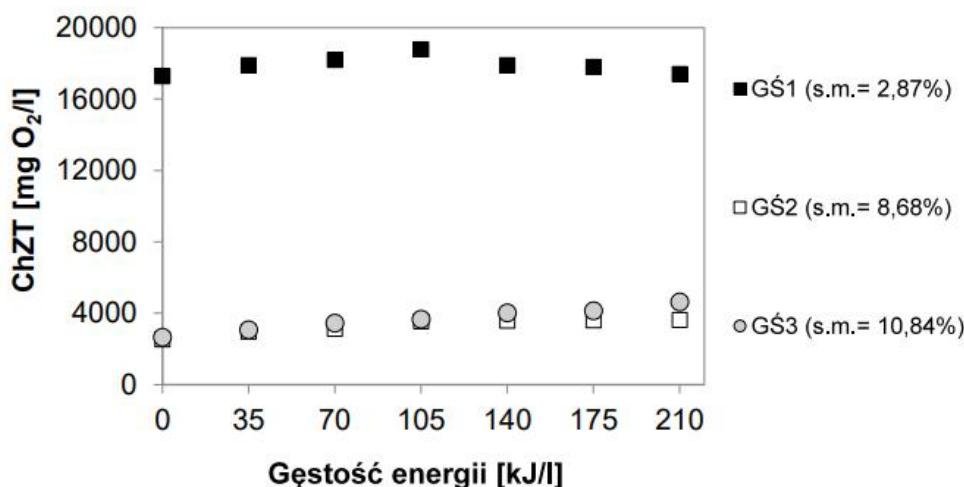


katarzyna.szmeichel@pw.edu.pl

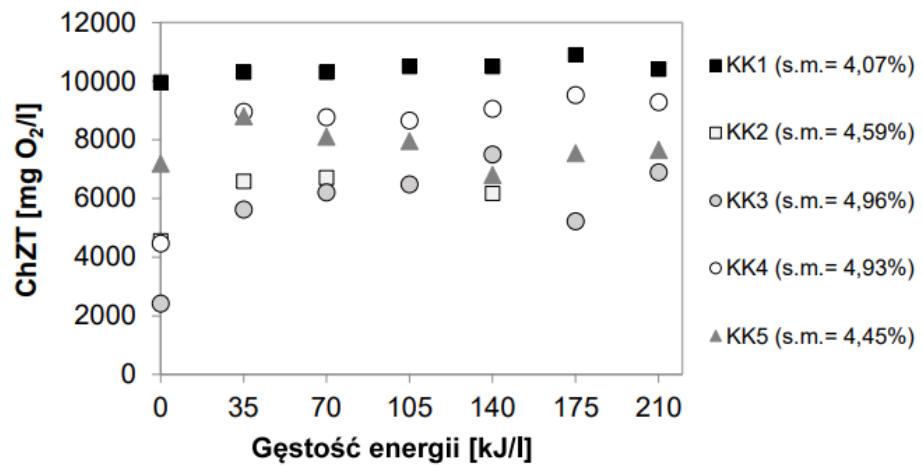
Development of a technology for preparation substrates used in methane co-fermentation by disintegration methods (DEZMETAN) No.: POIR.04.01.02-00-0022/17



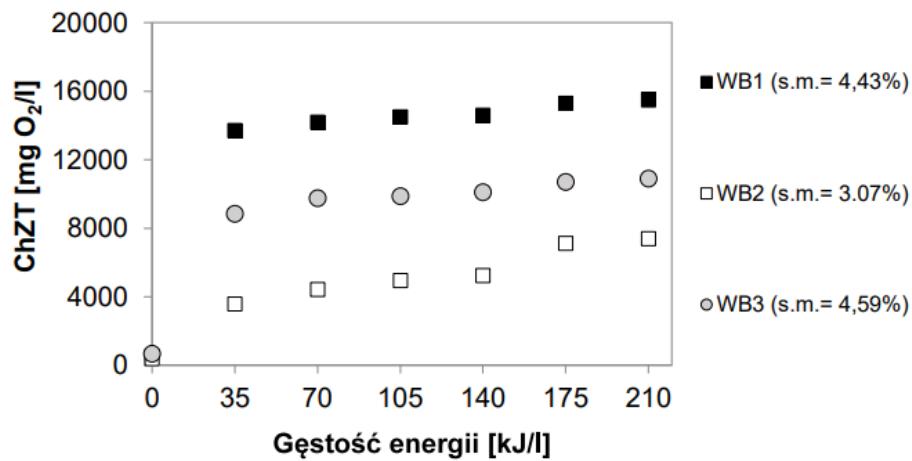
Rys. 4.4.27. Wartość rozpuszczonego ChZT gnojowicy bydlęcej w zależności od gęstości energii zużytej w procesie hydrodynamicznej dezintegracji.



Rys. 4.4.28. Wartość rozpuszczonego ChZT gnojowicy świńskiej w zależności od gęstości energii zużytej w procesie hydrodynamicznej dezintegracji.



Rys. 4.4.30. Wartość rozpuszczonego ChZT kiszonki kukurydzy w zależności od gęstości energii zużytej w procesie hydrodynamicznej dezintegracji.



Rys. 4.4.31. Wartość rozpuszczonego ChZT wysłodków buraczanych w zależności od gęstości energii zużytej w procesie hydrodynamicznej dezintegracji.