

# Valorization of rice husk chars as adsorbent: characterization and utilization in a novel reactor operating mode

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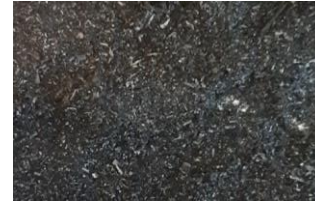


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# Rice husks

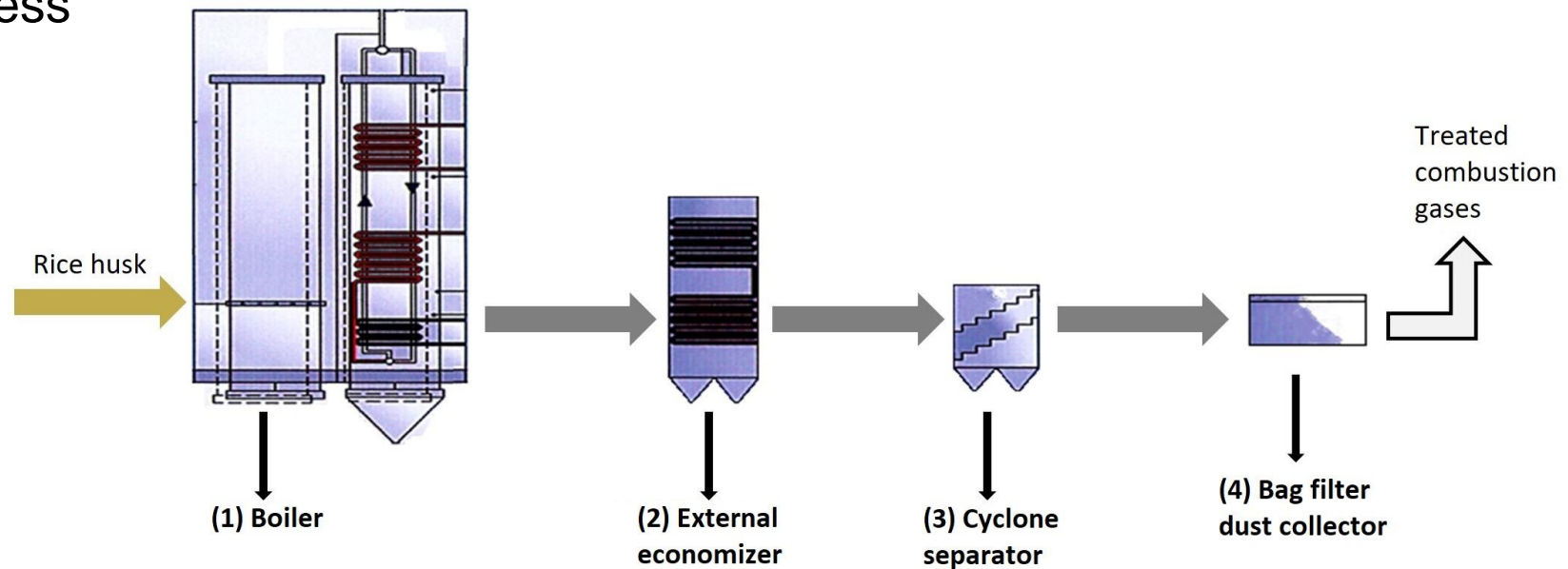
- Rice husks are incinerated to produce energy and steam

- Problem: Rice husk char



- Possible uses:
  - Silica production
  - Cement
  - Adsorbent

- Process



# Rice husks

- Rice husks are incinerated to produce energy and steam

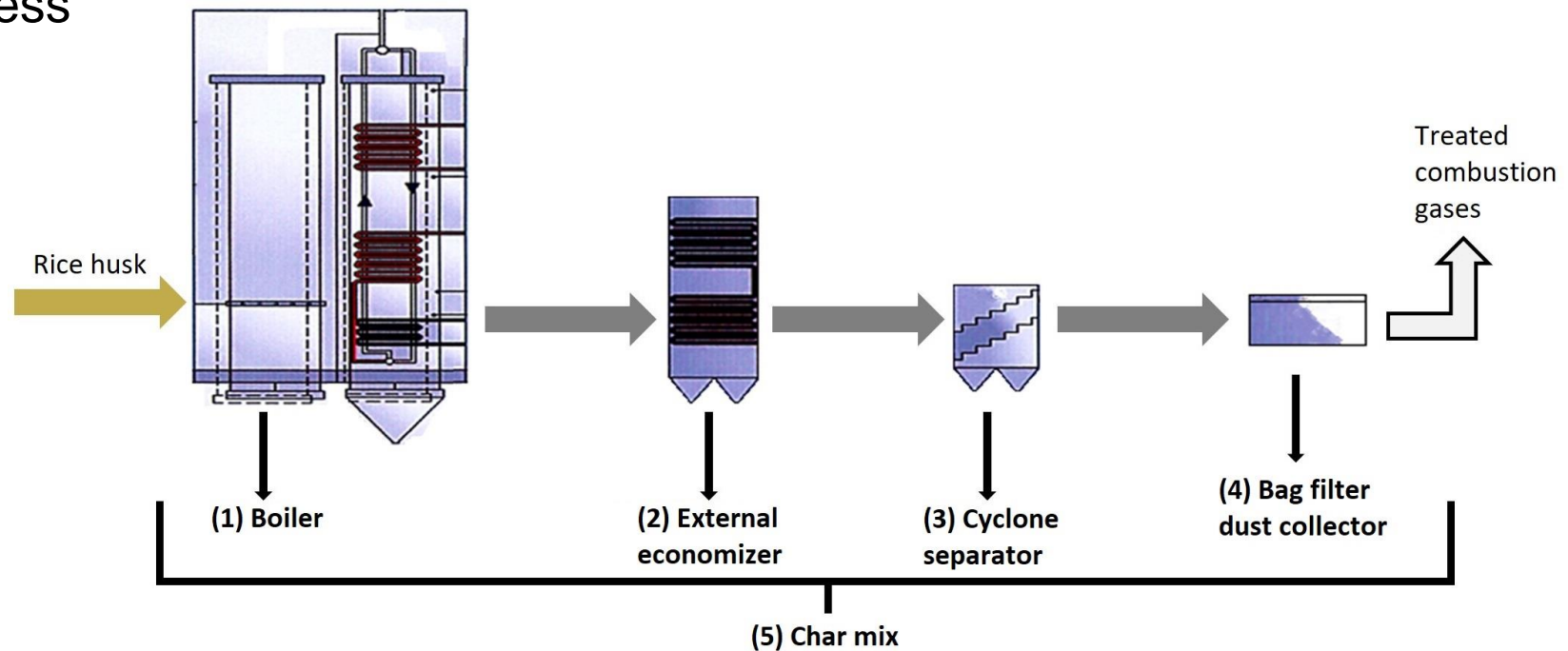
- Problem: Rice husk char



- Possible uses:

Silica production  
Cement  
Adsorbent

- Process



# Aims and objectives

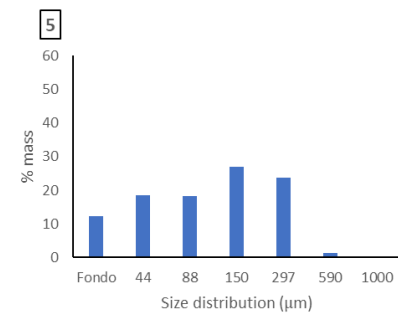
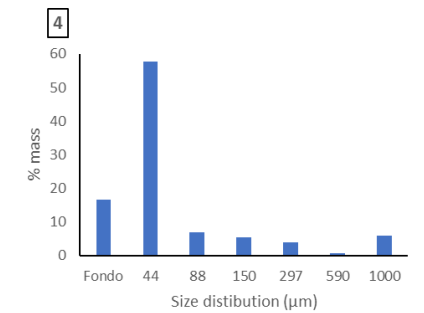
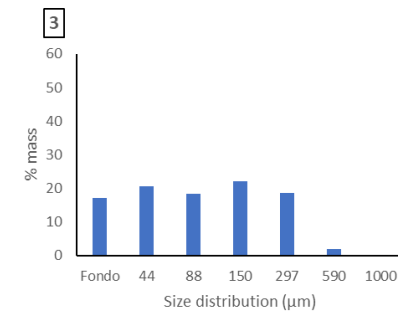
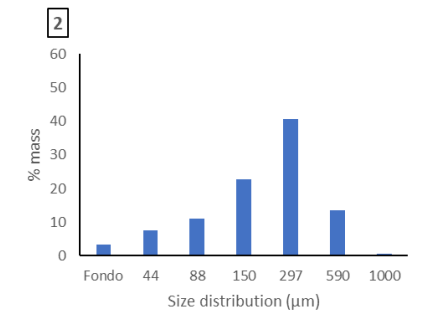
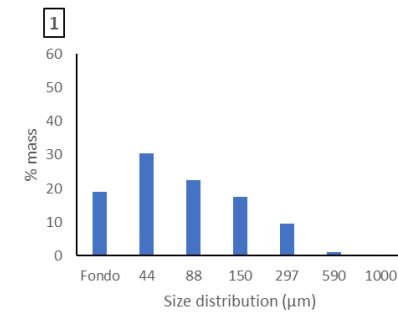
- Study the rice husk chars obtained in the industry as adsorbents to remove compounds from water
- Evaluate the use of the rice husk char in an adsorption reactor, and model its operation

# Characterization of rice husk chars

## Density

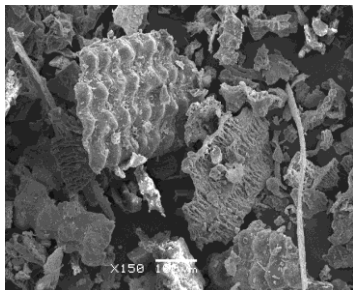
Char	Density (g/cm <sup>3</sup> )
Boiler (1)	0.37
Economizer (2)	0.15
Cyclone separator (3)	0.19
Bag filter (4)	0.21
Char mix (5)	0.19

## Particle size distribution (μm)

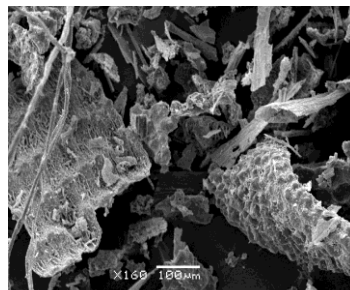


## Scanning electron microscopy (SEM)

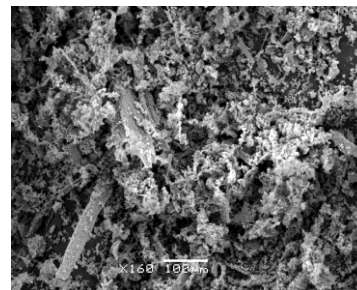
Boiler



Cyclone separator

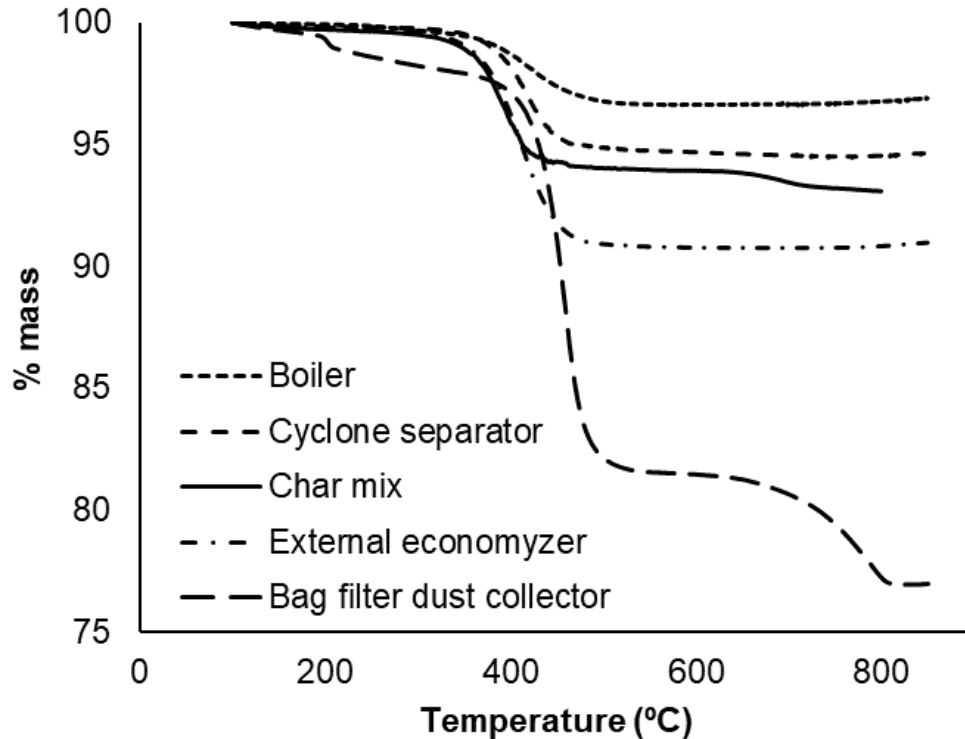


Bag filter



# Characterization of rice husk chars

## Termogravimetric analysis



## Energy dispersive spectroscopy (EDS)

Char	% C	% O	% Si	% Others
Boiler	1.7	43	40	15.3
Economizer	2.7	39	42	16.3
Cyclone separator	0.3	37	49	13.7
Bag filter	17	35	22	26
Char mix	n/d	44	43	13

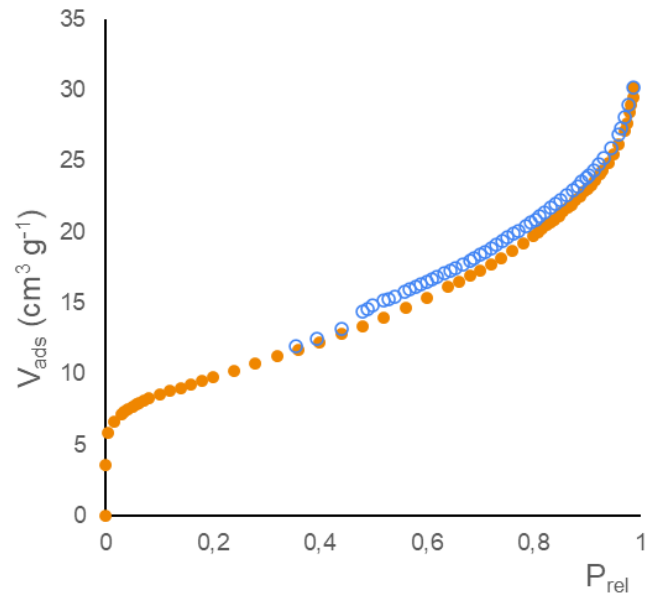
## Elemental analysis

Char	% N	% C	% H	% S
Boiler	0.00	2.84	0.58	0.00
Economizer	0.00	7.59	0.79	0.00
Cyclone separator	0.00	5.56	0.67	0.00
Bag filter	0.09	17.02	0.83	0.76
Char mix	0.00	5.89	0.60	0.30

% mass

# Characterization of rice husk chars

## BET area and pore volume



Char	BET area (m <sup>2</sup> / g)	Microporous volume (cm <sup>3</sup> / g)	Total pore volumen (cm <sup>3</sup> / g)
Boiler	11	0.0048	0.018
Economizer	56	0.011	0.055
Cyclone separator	54	0.01	0.06
Bag filter	45	0.071	0.075
Char mix	35	0.003	0.045

## X-ray diffraction (XRD)

Char	SiO <sub>2</sub>
Boiler	Crystalline
Economizer	Amorphous
Cyclone separator	Amorphous
Bag filter	Amorphous
Char mix	Amorphous

# Adsorption capacity / Adsorption kinetics

## Methylene blue

Initial concentration: 10 – 250 mg/L

Char: 100 mg

Volume: 50 mL

Char	$q_{\max}$ (mg/g)
Boiler	10.6
Economizer	42.4
Cyclone separator	28.2
Bag filter	56.5
Char mix	34.9
Activated carbon	126.9
Rice husk char (*)	246

## Phenol

Initial concentration: 10 – 1000 mg/L

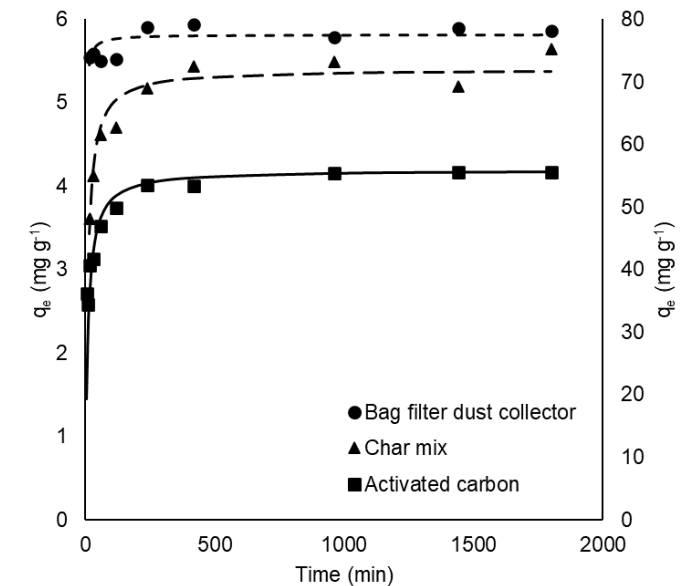
Char: 100 mg

Volume: 50 mL

Char	$q_{\max}$ (mg/g)
Bag filter	13.4
Char mix	8.3
Activated carbon	102

## Pseudo second order model

$$q(t) = \frac{q_e^2 k_2 t}{1 + q_e k_2 t}$$



	$C_0$ (mg/L)	$q_e$ (mg/g)	$k_2$ (g/mgmin)
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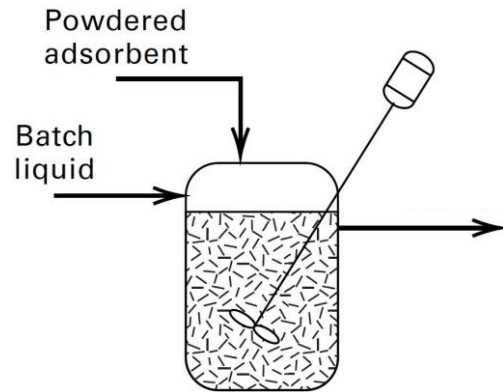
Phenol

Char mix	10	2.5	0.068
	20	2.79	0.0071
	50	5.52	0.013

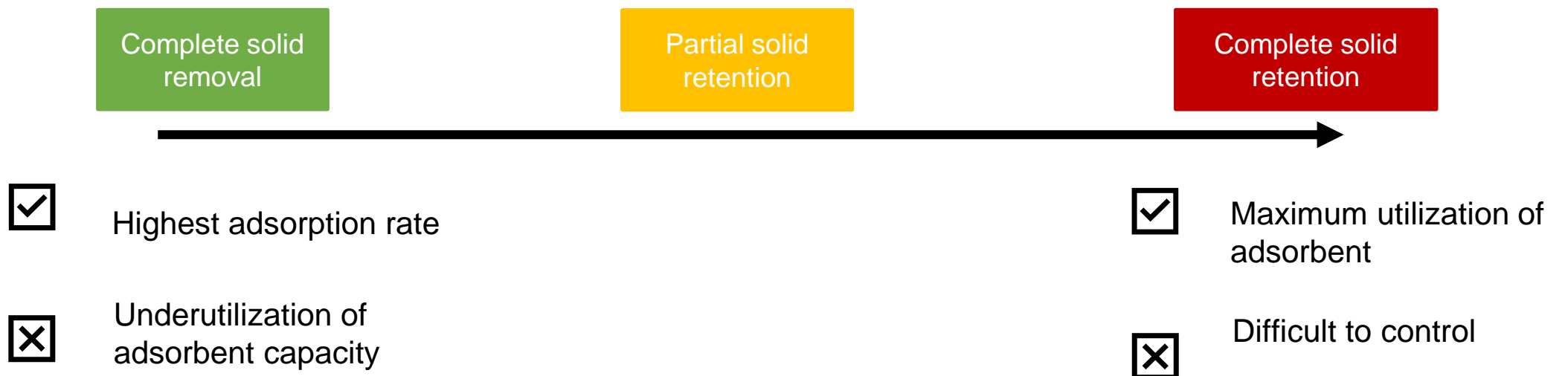
\* Lacuesta, J., *et al.* (2020). Rice Husk Bio-Chars as Adsorbent for Methylene Blue and Ethinylestradiol from Water. *Journal of Renewable Materials*, 8(3), 275.



# Stirred tank adsorption reactors-batch mode

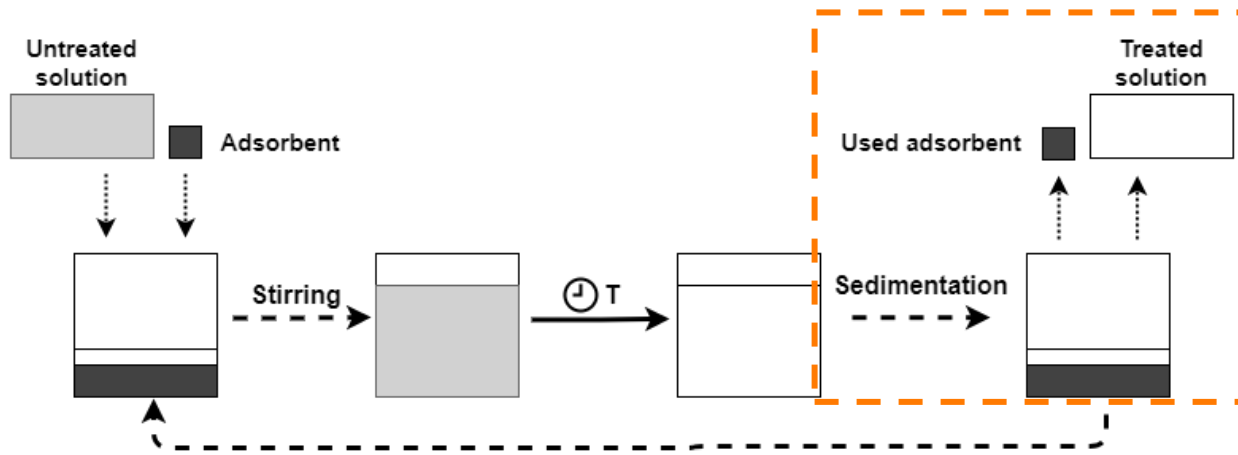


Seader et al (2011), *Separation Process Principles*



# Partially conserved batch (PCB)

Partial solid retention



$$f_m = \frac{m_e}{m}$$

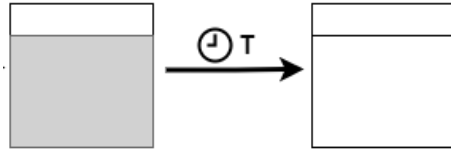
Fraction of adsorbent removed

$$f_v = \frac{V_e}{V}$$

Fraction of liquid removed

# Mathematical dynamic model

Cycle 1:



$$C_1(t) = C_0 - q(t) \frac{m}{V}$$

Initial concentration
Removed amount per volume at time  $t$

Cycle 2:

$$C_2(t) = \left( C_0 - q(T) \frac{m}{V} \right) (1 - f_V) + C_0 f_V - (q(t) - q(T)) \frac{m}{V} (1 - f_m) - q(t - T) \frac{m}{V} f_m$$

$$C_2(t) = \left( C_0 - q(T) \frac{m}{V} \right) \widehat{f}_V + C_0 f_V - (q(t) - q(T)) \frac{m}{V} \widehat{f}_m - q(t - T) \frac{m}{V} f_m$$

## Parameters

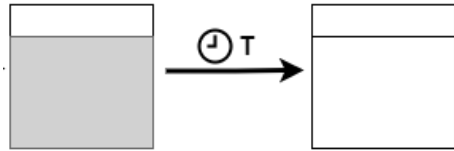
$C_0$	Initial concentration of the solution (mg/L)
$m$	Adsorbent mass (g)
$V$	Reactor volumen (L)
$m_e$	Adsorbent mass removed each cycle (g)
$V_e$	Treated solution volumen removed from the reactor each cycle (L)
$\widehat{f}_V$	$1 - f_V$
$\widehat{f}_m$	$1 - f_m$

## Variables

$q(t)$	Amount adsorbed at time $t$ (mg/g)
$C_i(t)$	Compound concentration inside the reactor during cycle $i$ at time $t$ (mg/L)

# Mathematical dynamic model

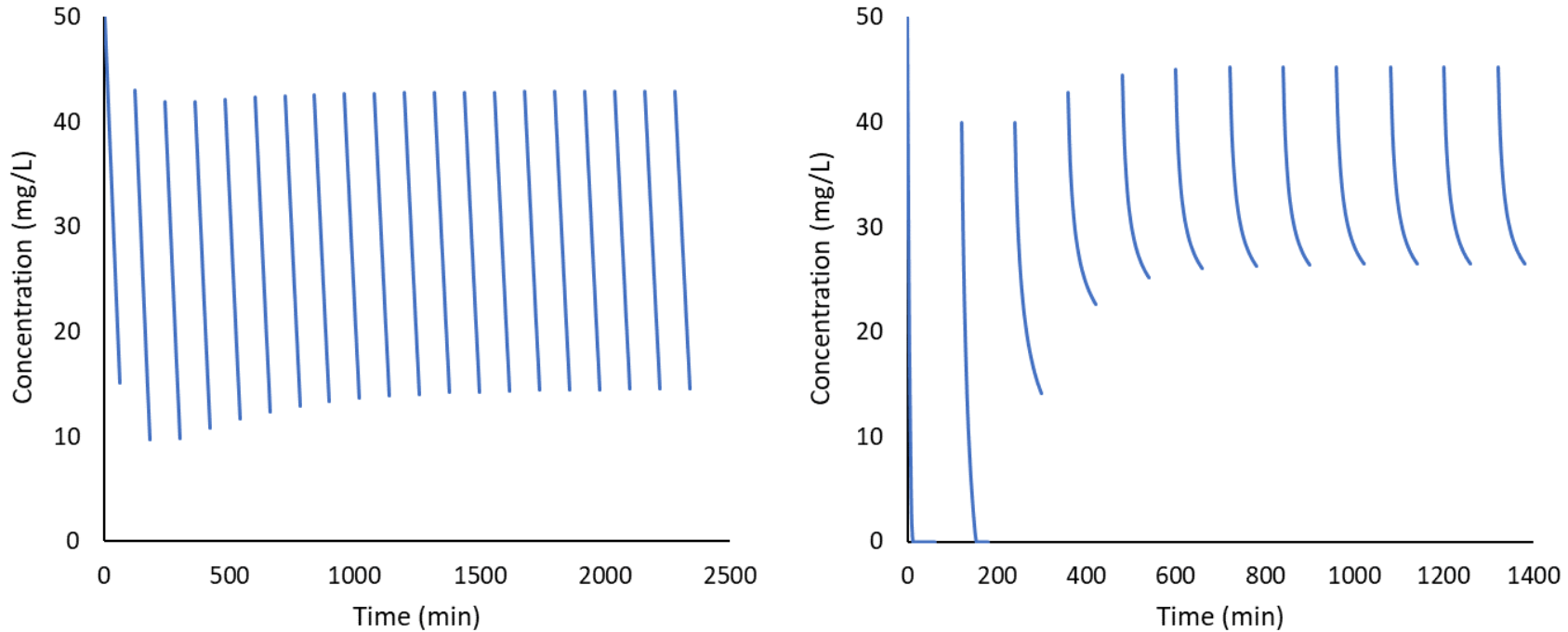
Cycle n:



$$\begin{aligned}
 C_n(t) = & C_0 \widehat{f}_V^{n-1} + C_0 f_V \sum_{j=0}^{n-2} \widehat{f}_V^j - q(T) \frac{m}{V} (\widehat{f}_V - \widehat{f}_m) \left( \widehat{f}_V^{n-2} + f_m \sum_{j=0}^{n-3} \widehat{f}_V^j \right) \\
 & - q(2T) \frac{m}{V} (\widehat{f}_V - \widehat{f}_m) \widehat{f}_m \left( \widehat{f}_V^{n-3} + f_m \sum_{j=0}^{n-4} \widehat{f}_V^j \right) \\
 & - q(3T) \frac{m}{V} (\widehat{f}_V - \widehat{f}_m) \widehat{f}_m^2 \left( \widehat{f}_V^{n-4} + f_m \sum_{j=0}^{n-5} \widehat{f}_V^j \right) \\
 & - \dots - q((n-1)T) \frac{m}{V} (\widehat{f}_V - \widehat{f}_m) \widehat{f}_m^{n-2} \\
 & - q(t) \frac{m}{V} \widehat{f}_m^{n-1} - q(t-T) \frac{m}{V} f_m \widehat{f}_m^{n-2} - q(t-2T) \frac{m}{V} f_m \widehat{f}_m^{n-3} \\
 & - \dots - q(t-(n-1)T) \frac{m}{V} f_m
 \end{aligned}$$

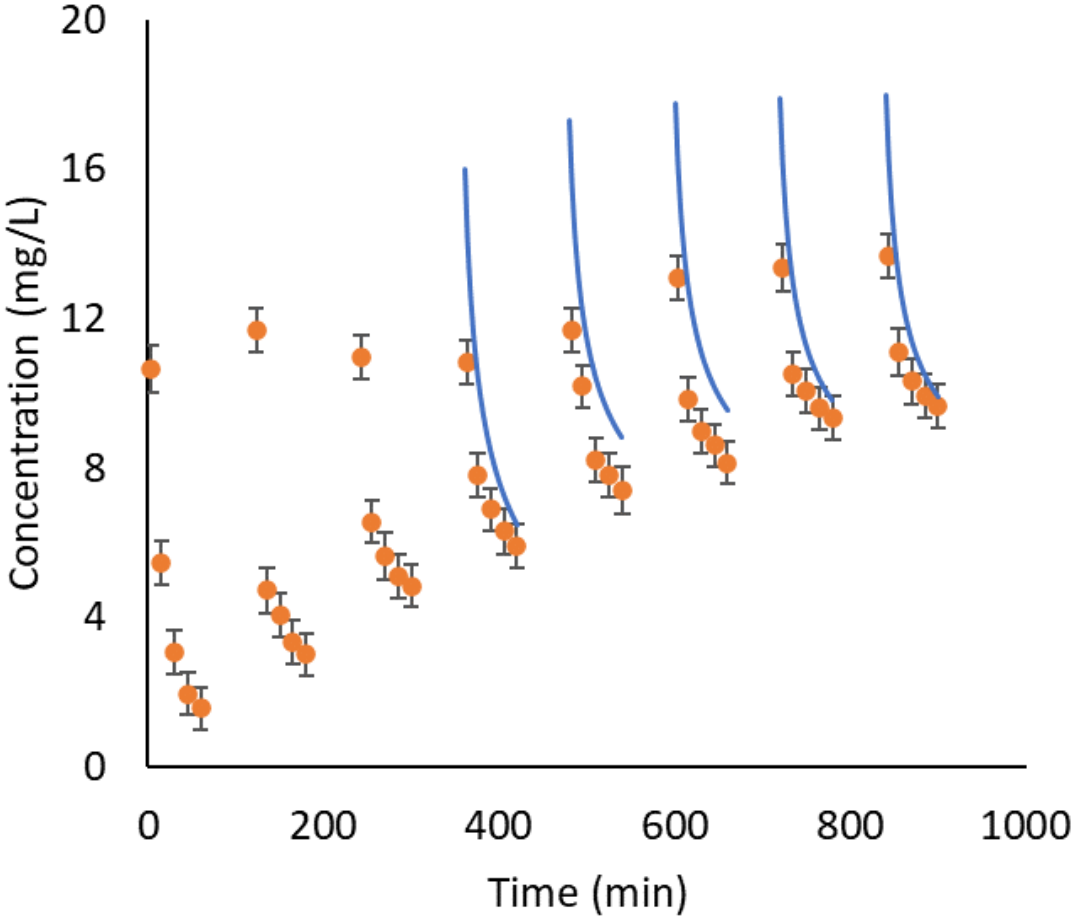
# Mathematical dynamic model

Considering the two most common adsorption kinetic models (pseudo first order -left- and pseudo second order -right-), the concentration inside the reactor is presented:



After several cycles the concentration at the end of each cycle does not change

# Lab scale experiment



# Periodic final concentration ( $C_p$ )

- Pseudo first order (PFO)

$$C_p(T) = C_0 - \frac{m f_m q_e (e^{kT} - 1)}{V f_V e^{kT} + f_m - 1}$$

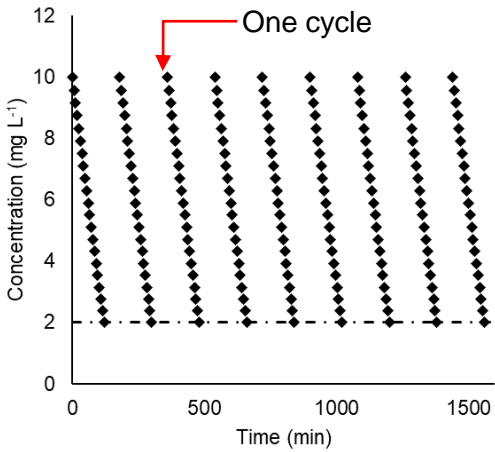
- Pseudo second order (PSO)

$$C_p(T) = C_0 - \frac{m f_m^2}{V f_V} \sum_{j=1}^{\infty} \left[ \frac{q_e^2 k j T}{1 + q_e k j T} (1 - f_m)^{j-1} \right]$$

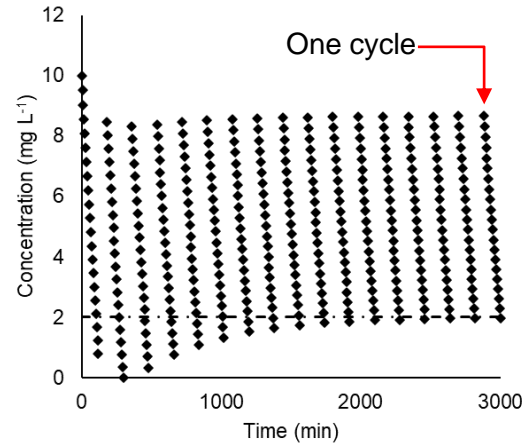
- Simulation: Calculate  $C_p$ , knowing  $C_0$ ,  $m$ ,  $V$ ,  $f_m$ ,  $f_V$ ,  $T$
- Design of the PCBr: calculate reactor operating parameters ( $m$ ,  $V$ ,  $f_m$ ,  $f_V$ ,  $T$ ) to obtain a set value for  $C_p$

# Comparing different operating modes

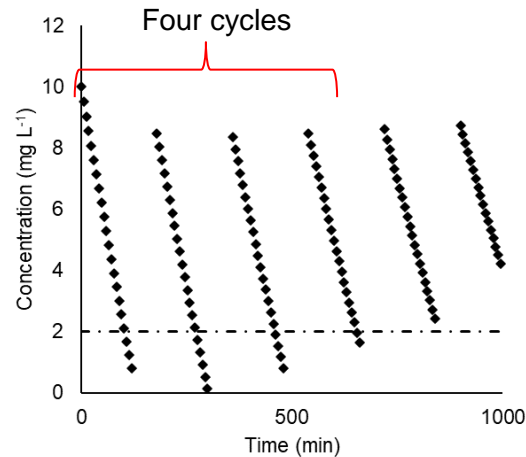
Complete solid removal



Partially conserved batch



Complete solid retention



	Complete solid removal	Partially conserved batch	Complete solid retention
Initial adsorbent mass (kg)	63	72.6 (calculated using $C_p$ equation)	72.6
Adsorbent added (kg)	63 (one cycle)	14.5 (one cycle)	72.6 (four cycles)
Adsorbent mass added per unit of treated water ( $\text{kg m}^{-3}$ )	0.420	0.116	0.145

$f_V$	1	5/6	5/6
$f_M$	1	1/5	0

$V = 150 \text{ m}^3$   
 $T = 2 \text{ h}$



# Conclusions

- Rice husk chars have different adsorption properties depending where they are generated
- Rice husk chars can be used to remove compounds from water
- The proposed reactor operation allows to better control the adsorption process, and can reduce the adsorbent mass used

# Thank you for your attention!

## ACKNOWLEDGEMENT

