## Energy recovery of waste using incineration process

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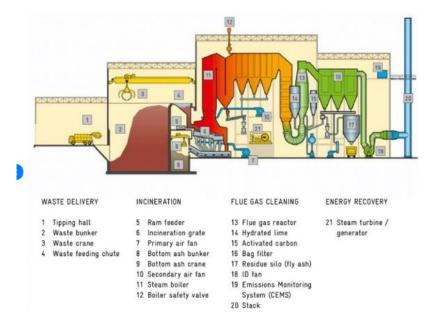
## Introduction

In light of the ambitious goals set by the National Waste Management Plan (Ministerial Decision 30 31.8.2020 Government Gazette 185/A 29.09.2020) promoting the development of Energy from Waste plants (EfW), combustion seems the most viable solution for the treatment of residual waste albeit public objections. An opportunity has arisen given the circumstances; including the introduction of the Landfill tax which would make energy recovery cheaper than Landfill disposal, the decarbonization strategy as well as the energy and fuel crisis seeking for renewable energy sources and the goals set by the government to minimise coal usage. This study neither adds any information on optimising operational parameters nor questions the proven and robust operating technological principles of an Energy Recovery Facility (ERF). This report provides an overview of how an ERF operates and highlights various operational issues that need to be considered by the operator.

## Discussion

A state of the art EfW with an annual capacity of 400.000 tonnes operating in 2 processing Lines of roughly 25 tonnes/hr has a capital investment cost of roughly 120.000.000<sup>1</sup>. A typical ERF operates approximately 7.800 hours annually circ. 90% availability. To reduce downtimes and operational issues, an Outage period for maintenance activities is scheduled, usually taking place twice per annum with a duration of 2 weeks. The operational cost varies depending on the capacity of the unit due to economies of scale eg 100.000 at per tonne 65, 200.000 at 45 per tonne. The operator on behalf of the waste disposal authority would be overcovering the EfF operational costs including the treatment, maintenance and disposal by the gate fee. Additionally, the operator would have additional sources of profit. The operator would charge the authorities for the electricity that would be exported to the grid ie on the scale of a 400.000 tonnes per annum facilities could be exporting a net electrical power of 34,7 MWth<sub>el</sub> considering parasitic loads. Additionally as an ERF encompasses a CHP infrastructure the operator would be charging the authorities the steam exported to nearby facilities ie 65 tonnes/hr of Intermediate Pressure steam of 16 bar, 236C or the steam distributed at a lower range to district heating networks. Given the arrangements in place ie the use of vibrating tables, overband magnets or drums the operator could make additional profit secondarily from the metals that could be recovered from the bottom ash fraction. Figure 1 gives an outline of how a typical ERF operates and it's main stages.

<sup>&</sup>lt;sup>1</sup> Please, note that all the figures are provided in sterling pounds (£) currency, base year 2013



**Figure 1** An overview of the plant operations pointing out the inputs and the outputs of the incineration process. The whole process starts from the Tipping Hall were waste is disposed and fed with cranes to the grate. Flue gas is generated that heats up the water in the boiler. When the saturated steam reaches it's superheated properties in the Superheater section, it is driven to the Turbine and turned to electricity that is exported to the grid as well as heat that is extracted from the Turbine to be utilised via pipework to district heating networks and nearby facilities. Part of the remaining heat is absorbed at the boiler part by the Economiser bundles. The Economiser bundles are cooling down smoothly the flue gas to reach the proper Temperature to enter the FGT setion. In the FGT part the flue gas with a series of chemical addition inside a scrubber and a bag filter it exits the stack. CEMS monitors the flue gas performance to make sure that it is free from harmful contaminants. The ash and APCr are disposed as appropriately. Their disposal is subject to strict monitoring surveilance.

As part of the maintenance activities and the annual maintenance plan, by law there are requirements for periodic inspection and testing of Pressure Equipment by the competent authorities, checks of the steam boiler, expansion valves and so on. Additionally, preventative maintenance shall cover calibration of measuring equipment, regular periodic inspections, e.g. Non Destructive Tests (NDT) and inspections of the heat exchangers part for wear ie measuring the thickness of heat tube exchangers, replacement of refractory materials, regular cleaning of parts ie the boiler, tensioning belts, lubrication of moving parts, filters change and parts of the auxiliary equipment ie lifting beams to be inspected by notified body etc. An overview of the boiler Outage activities is highlighted in Figure 2. Outage covers the Worker Orders that can be conducted as appropriately. The primary objective is to run the plant at the highest availability and offset any downtime costs. These so called Work Orders are presented in Figure 3A.

In addition to preventive maintenance requirements, there are ongoing issues that require continuous monitoring and frequent attention while being online ie treatment of blockages. As part of the plant daily operation routine, the operator must monitor a number of critical issues to ensure maximum availability, energy utilisation and compliance. Therefore, critical parameters have been set to be monitored. Each shift before starting does the necessary checks including plant equipment and by the end of the shift, reports critical issues as part of the shift handover process. Plant performance is tracked on the daily operations report. Figure 3 B depicts a number of issues the operator deals with on a daily basis.

	On Load	Durati	-	
	Cancel permits & de-isolate	Conati	on Start	Finish
		48 hrs	Sat 08/04/17 19:0	
28	i ve deat	6 hrs	Sat 08/04/17 19:0	
6	Start up turbine and export power	6 hrs	Sun 09/04/17 01:0	
12	The Durage Une & Cool Drive	36 hrs	Sun 09/04/17 07:0	
3	Pre-Outage Line 4 Cool Down	0 hrs	Mon 10/04/17 19:0	
4	Off Waste	22.60	10/04/17 19:0	00 Mon 10/04/
6	Cool down period	9 days	Wed 29/03/17 19:0	10  SIL01/04/1
7	Permit prep & isolations	0 hrs	Wed 29/03/17 19:0	
	Line 4 Engineering Work	60 hrs	Wed 29/03/17 19:0	
1	Engineering Works	12 hrs		00104/1/
2	Furnace, Boiler & Pressure Parts	and her	Sat 01/04/17 07:00	Sət 01/04/17
3	Furnace External	414 hrs	Sat 01/04/17 07.00	Tur 18/04/1
5	Open all former	411 hrs.	Sat 01/04/17 07:00	Tue 18/04/17
6	Remove blocks	2.5 hrs	Sat 01/04/17 07:00	Tue 18/04/17
7		1 hr	Sat 01/04/17 07:00	Sat 01/04/17
8	Check clinkers via level 9 doors	1 hr	Sat 01/04/17 07:00	Sat 01/04/17 0
10	Furnace	0.5 hrs	Sat 01/04/17 08:00	Sat 01/04/17 0
11	Rope access to remove clinkers 1st pass	360 hrs	Sat 01/04/17 09:00	Sat 01/04/17 0
	Install bridge & hand rail	5 hrs	Sat 01/04/17 19:00	Sun 16/04/17 1
12	Install furnace lighting	2 hrs	Sat 01/04/17 19:00	Sun 02/04/17 0
13	Internal clinker inspection	30 mins	Sun 02/04/17 07:00	Sun 02/04/17 05
14	Clean grate (ash extractor running and arb grate is such a	30 mins	Sun 02/04/17 09:00 Sun 02/04/17 09:30	Sun 02/04/17 09
15	Clean grate (ash extractor running and ash grabs in auto) - To include a jet wash of all tiles (screening to be installed Grate snots - "Out" stroke	5hrs		Sun 02/04/17 10
16	Install 1st pass scaffold	4.5 hrs		Sun 02/04/17 15:
17	Hard clean of existing inconel	9 hrs		Sun 02/04/17 19:
18	Grit blast 1st pass existing inconel	3 hrs		Mon 03/04/17 16:
19	Clean down scaffolding - 1st pass	12 hrs		Mon 03/04/17 19:
20		1 hr		ue 04/04/17 07:0
21	Refractory inspection above and below the prism, to include feeding table area Mobilise refractory company	2 hrs	the second se	ue 04/04/17 08:00
22	Set up of equipment for refractory works (external)	0 hrs		e 04/04/17 10:00
		9 hrs		e 04/04/17 19:00
23	Grit blast 1st pass existing inconel	12 hrs		ed 05/04/17 07:00
24				d 05/04/17 08:00
25		11 hrs	Wed 05/04/17 08:00 We	d 05/04/17 19:00
26			Thu 05/04/17 08:00 Thu	06/04/17 10:00
27				06/04/17 19:00
28	herberg words shirts			7/04/17 07:00
29	nervectory north and the			7/04/17 19:00
30				8/04/17 07:00

Figure 2 Typical Outage breakdown

430	Inspection and repair of fault	6 hrs	Wed 22/03/17 08:00	Wed 2
431	Lagging to be installed	6 hrs	Fri 24/03/17 09:00	Fri 24/0
432	Scaffold removal	28 hrs	Mon 27/03/17 08:00	Tue 28
434	HV works, inspection maintenance & testing	6 hrs	Tue 28/03/17 12:00	Tue 28
435	General lighting external	96 hrs	Sun 02/04/17 07:00	Thu 06/
436	General lighting internal	0 hrs	Tue 21/03/17 08:00	Tue 21/
437	Work Orders & Defects	0 hrs	Tue 21/03/17 08:00	Tue 21/
438	Pressure gauge slight steam leak on pipework - 565470- 23LBA10CP510QP01	72 hrs	Tue 21/03/17 07:00	Fri 24/0
439	Gland repack and valve overhaul - 23LBA10AA002N	12 Res	Tue 21/03/17 07:00	Tue 21/
440	Boiler house Ivi 5 - sight glasses require maintenance - 23HAD10CL5100P01	12 hrs	Tue 21/03/17 07:00	Tue 21/
441	leak from rear door of ash extractor line 3 left - 23HAD10CLS100P01	12 hrs	Tue 21/03/17 07:00	Tue 21/
442		12 hrs	Wed 22/03/17 07:00	Wed 22
443	Steam leak reseal and Furmanited flange repair - 23LAE11BRXXXXX	12 hrs	Tue 21/03/17 07:00	Tue 21/
	Hydraulic ram is leaking oil from the seal - 23HHC10AE002	12 h/s	Tue 21/03/17 07:00	Tue 21/
444	Correcting the wiring to the motor pillar - Defect 66	36 hes	Tue 21/03/17 07:00	Wed 22,
445	FF0880 Halton work packs P2WP 390 and 391	36 hrs	Tue 21/03/17 07:00	Wed 22,
446	Damper will not close - 23HLA60AA002F	12 hrs	Tue 21/03/17 07:00	Tue 21/
847	Inspect double dump valve condition - 23ETG14AA020-S01	6 hrs	Tue 21/03/17 07:00	Tue 21/
448	Inspect double dump valve condition - 23ETG14AA020-S01	6 hrs	Tue 21/03/17 07:00	Tue 21/
149	Overhaul and test boller level gauge - 23HAD10CL510QP01	72 hrs	Tue 21/03/17 07:00	Fri 24/0
ISO	leaking gland - 23QKD15AP001	12 hrs	Tue 21/03/17 07:00	Tue 21/
51	Suspect dust leak on bags - 23RJC18CL301-F01	12 hrs	Tue 21/03/17 07:00	Tue 21/
\$2	Suspect dust leak on bags - 23RJC15CL301-F01	12 hrs	Tue 21/03/17 07:00	Tue 21/
		12 hrs	Tue 21/03/17 07:00	Tue 21/
3	Suspect dust leak on bags - 23RJC11CL301-F01	24 hrs	Tue 21/03/17 07:00	Wed 22
4	Drain valve overhaul required - 23HANXXBRXXX	72 hrs	Tue 21/03/17 07:00	Fri 24/0
	Under grate U tube water leaks - 23QKC428R012C	72 hrs	Tue 21/03/17 07:00	Fri 24/0
	Lindes mate II tube tile connector leaks and sheared bolt - 23QKC420RU13C	6 hrs	Tue 21/03/17 07:00	Tue 21/
	Pin on Actuator Clutch is bent and sticks in when depressed in - 23LBA10AA002N-M01	Units		
		Page 10		

Name				Fri 10/11/17 11:00	Fri 10/11/17 15:00
	11GHF30A4001X - Line 1 - blow down tank process water control valve - Boiler House (P1/2), Boiler	Hall,Level 00m	4 hrs	FILTOLEVEL LEGO	
	(Bottom Ash Conveyer) Line 01 IHAC11AC001 - Line 1 BFW to economisers 3-way valve (11HAC10AA001X) is leaking up spindle -		4 hrs	Fri 10/11/17 15:00	Fri 10/11/17 19:00
	(P1/2),Boiler Hall,Level 29.2m (Superheater/Economiser access),Line 01 (1HAD10CL510QP01 - Line 1 boiler drum sight glass leaking, - Boiler House (P1/2),Boiler Hall,Level :		4 hrs	Fri 10/11/17 19:00	Fri 10/11/17 23:00
	Drum),Line 01 1HAXXBRXXX - Level 1, pipework on ceiling running from hydraulic skid room phase 1/2 leaking fro		4 hrs	Thu 16/11/17 15:00	Thu 16/11/17 19:00
	House (P1/2),Boiler Hall,Level 06m (Furnace/Grate),Line 01 11HHC10AE001 - Replace hydraulic cylinder - Boiler House (P1/2),Boiler Hall,Level 06m (Furnace/Gr		4 hrs	Fri 17/11/17 07:00	Fri 17/11/17 11:00
	11HHC30AA001M - Grate cooling leak element 3 - Boiler House (P1/2),Boiler Hall,Level 06m (Furna		4 hrs	Fri 17/11/17 11:00	Fri 17/11/17 15:00
	01 11HHC30AE001 Replace hydraulic cylinder - Boiler House (P1/2),Boiler Hall,Level 06m (Furnace/G		4 hrs	Fri 17/11/17 15:00	Fri 17/11/17 19:0
	11HHC40AE001 - Replace hydraulic cylinder - Boiler House (P1/2),Boiler Hall,Level 06m (Furnace/G	ate),Line 01	4 hrs	Fri 17/11/17 19:00	Fri 17/11/17 23:0
	11HLB60AN001 - Planned routine maintenance - Boiler House (P1/2),Boiler Hall,Level 14.6m (Fly As 01	h Conveyor),Line	4 hrs	Sat 18/11/17 11:00	Sat 18/11/17 15:0
,	111BA10AA002N - On/off valve leaking from body - Area cordoned off level 8 boller house - Boller I (P1/2),Boller Hall,Level 29.2m (Superheater/Economiser access),Line 01	louse	12 hrs	Sat 18/11/17 15:00	Sun 19/11/17 03:
1	11QKC43BR011C - R/h side cooling water hose no. 5 element 3. Leaking - Boiler House (P1/2),Boile 10.95m (Furnace Feeding Table).Line 01	Hall,Level	2 hrs	Sun 19/11/17 03:00	Sun 19/11/17 05:
Post Ou	atage Line 1 Start Up	State of the local division of the	72 hrs	Mon 20/11/17 19:00	Thu 23/11/17 19:
Post	Outage Line 1 Start Up		3 days	Mon 20/11/17 19:00	Thu 23/11/17 19
	ancel Permits & De-isolate plant		12 hrs	Mon 20/11/17 19:00	Tue 21/11/17 07
	re-Heat		60 hrs	Tue 21/11/17 07:00	Thu 23/11/17 19
0	On Waste			TL 22/11/12 10 00	

Figure 3A Work Orders are executed, defects are rectified, changes are implemented during the Outage as a window of opportunity arises

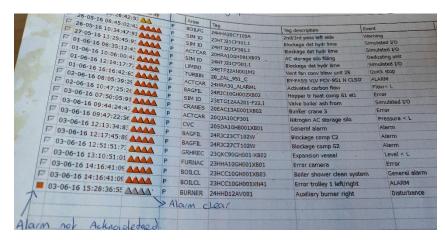


Figure 3B A number of alarms on the plant's critical parameters been monitoed listed as part of the operator's daily routine

Training and supervision have been provided by the EPC, however equipment defects and issues could not always be claimed under contracts, as the EPC might prove that these failures are attributed to operational misuse. Although the contractor has provided the operator with the necessary warranties e.g. 40.000 guaranteed hours of operation for a type of heating tubes and the number of critical spare parts required, many times wear resulting from omissions or failures by the operator, e.g. not properly monitoring the demineralised water, ineffective cleaning of soot deposits etc. can halve lifespan of tubes. An indicative part of a critical spares inventory list is given in Figure 4 considering the spares consumption and lead times.

Lifetime of tubes at elevated temperatures is reduced exponentially and relatively to the Temperature drifting, resulting in thinning of tubes which has a knock on effect on the steam boiler and on plant operations. Frequent breakdowns in the feeding system ie failure of the cranes can hinder the grate supply. The level of water in the Boiler Drum could cause operational issues. The non-calibration of measuring equipment could lead to operational parameters drifting and major operational control issues. The damage of the cooling system in a water-cooled grate could cause the fast reduction of the grate tiles lifespan. The ineffectiveness of boiler cleaning e.g. insufficient Pressure on rapping gear system in the heat exchangers section, or the interruption of cleaning flow on the shower cleaning system, could lead to fouling, transfer heat inefficiencies, thinning and wear to the heat exchanger tubes. The deficient monitoring of water quality could cause scale, deposition attack, scabbing, pitting and cracks to the tubes and other parts of the plant by carry over. Auxiliary Burners failure, the non-calibration of the Continuous Emissions Monitoring System (CEMS), the incorrect supply of chemicals ie NH3 solution or failure of equipment ie SNCR supply, may result in abnormal operation and could result in environmental fines. Figures 5, 5A till K illustrate a number of critical issues that must be monitored regularly.

MANUT	PARYN	GETALES SPECIFICATION	off/ Bard	610 (M)	1995 BEV Vinger E. Logeller	1079 #2.5.10
Fastural Margar	87546 Jan (H. JS4J	Represent insuring for analog cut	Fasma	1		1.60
Reserve	67015 236 51 3002	Grate the	3 rows pr		TOTAL AL TOP	
Pression	ST015 238 01 1002	Grane tee	2000	and the second second	laman a lam	1 .
Repairied	97010_336_31_1665	Date and the left	1 900		lemeral a low	1.
Rossear	STORS_236_D1_LOSA	Units wall the last	1 -	- 1-	Lamaral + Lan	1.
Remained	ST015 396 01 1062	Side wat the right	1 -			
Researce	67010,296,81,1062	Side and the regist			and a lateral	
NP UP	117014 Jun (71 pous	Gunting profile for suggest along	1		WEAN A LOS	
(Mr.UP)	67014 239 pt 2644	Guiding plate for support all-ad	1		WEAR + THE	
Brun.	87014_338_01_2003	Buppenting advant dar 180 mm (editoret alvergalases)	bollar	Neine	VIEL + MASIN	
SPUP	87614.238.01,7054	Supporting advant constant (authous) primplatase &	testaj	None	ace to farming	
BPU/P	87014 238 S1 7058	Eductor isfant die 150 mm (ausenbilij		1	WEAR & IDO	
				+	1 1 1	1

Figure 4 Part of the critical spares list inventory supplied by the EPC which is monitored by the operator considering the spares consumption and lead time

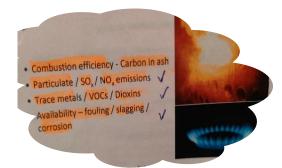
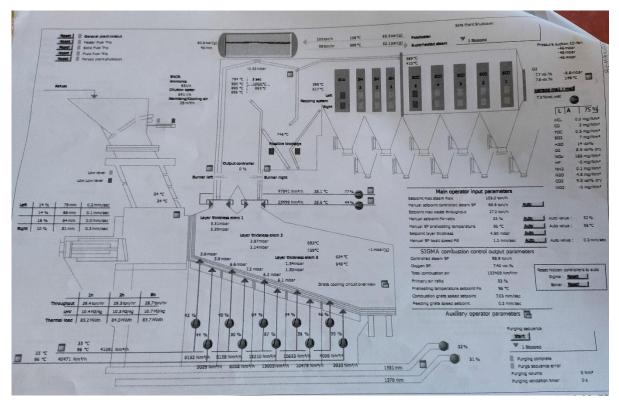


Figure 5 Indicative key operational parameters which must be monitored



Figure 5A Waste cranes operation might be hindered as a result of stresses generated by the crane's movement at different angles and the diverse nature of waste composition leading to failures



**Figure 5B** DCS screen of the Furnace and Boiler section indicating critical operational parameters including the waste throughput, the Calorific Value, the waste layer of thickness, the Primary and Secondary Air, Temperature probes monitoring the 2 seconds combustion compliance, the Boiler Drum Level etc.

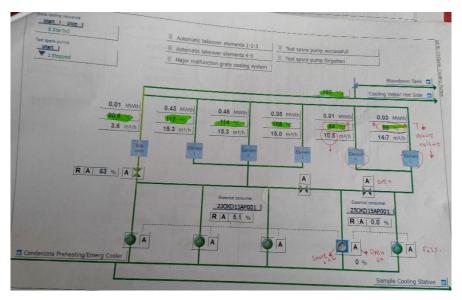


Figure 5C DCS screen of grate cooling system

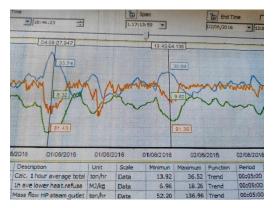


Figure 5D DCS extracted graph indicating the corelation between Calorific Value the orange line, waste throughput the blue line and HP steam production the green line

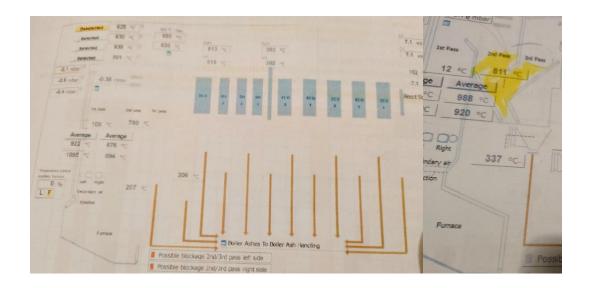


Figure 5E DCS screen on the Boiler side highlighting the 2<sup>nd</sup> and 3<sup>rd</sup> pass narrow passage

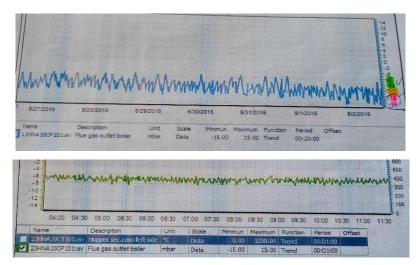


Figure 5F DCS extracted graphs of flue gas path monitoring. The optimal operational range lies within -6 to -8 mbar

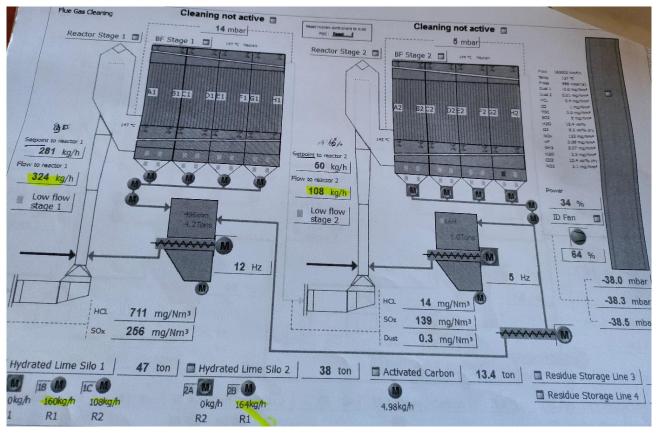


Figure 5G DCS layout monitoring the FGT section

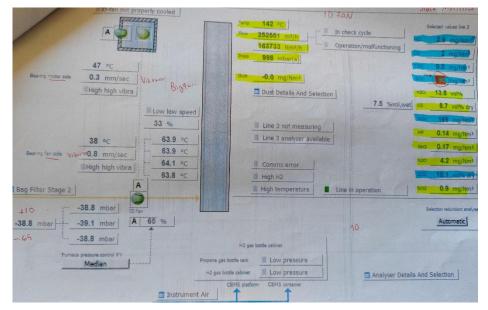


Figure 5H DCS layout monitoring ID Fan and emissions monitoring system



Figure 5I Boiler Drum Level Indicator

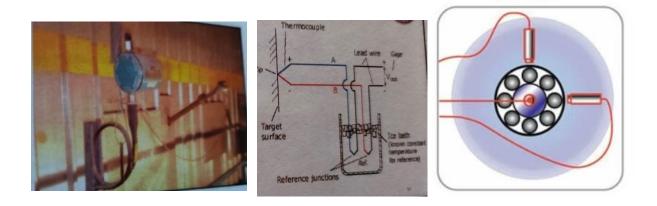


Figure 5 J1 Measuring equipment and condition monitoring techniques been used

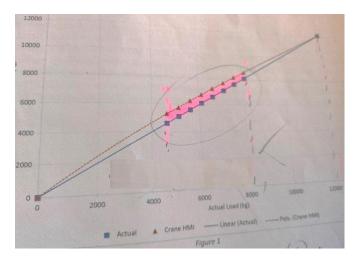


Figure 5 J2 Waste Cranes load cells quarter callibration regime against calibrated weighbridge carried out with the use of load tests. Calibration results to be plotted to monitor inconsistencies of drifting between the DCS values and the actual operating envelope



Figure 5K Continuous Emissions Monitoring System (CEMS) working principle and requirements against EN 14181

The purpose of the EfWs following the waste hierarchy is to recover the non recyclable waste which would otherwise been driven to Landfill for subsequent disposal. Although incentives are given for the use of recyclates as a raw material to Producers converting recyclates into new materials thereby reducing the usage of virgin raw materials including plastics, there can be issues and unforeseeable events that pose challenges. In a constantly changing and highly adaptive market with many drivers affecting the supply chain ie prices, purity protocols, China waste Ban policy effect etc. it is not always possible for the Producers to use all the recyclates as a raw material and as a result would create recyclate streams disposed to Landfill. Based on the legal framework under the extended producer's responsibilities obligation system the use of energy recovery can be used complimentary for the waste fraction that cannot be recycled based on the Article 10 of the Waste Framework Directive 2008/98/EC.

Primarily non-hazardous Municipal Solid Waste (MSW) and similar waste may be fed to the incinerator. The grate type that has predominantly been used, is the moving grate technology one. It's widespread application relies on the robust design and it's technological advanced features. The moving grate has been built in a manner that allows the feeding of unprocessed waste. The untreated waste offers in theory several benefits including the avoidance of treatment costs and the processing of a wider range of feedstock. By doing so, the operator is provided with more benefits and flexibility however, there is a number of limitations that shall be considered. By the diverse nature of the treating waste and the incineration practice, combustion could create several issues to mechanical equipment, frequent blockages, unstable operation due to inhomogeneous calorific value, non-combustible materials coming of the bottom ash, while they could also create pollution problems. Waste that by its state is non hazardous ie plastics a predominant type of non hazardous waste that is common in the refuge which offers a good heating value, during the burning process it releases harmful pollutants such as high Cl, S emissions. Figure 6 indicates the different combustion Temperature range of the various waste feedstock used as well as the associated formation of hazardous flue gas contaminants and treatment.

The recovered biodried RDF or certified SRF gives more confidence to the operator as it follows a standard regime which requires routine sampling procedures and monitoring laboratory analysis based on Ministerial Decision 56366/4351/2014, Government Gazette 3339/B' 12.12.2014. By doing so the feedstock is certified for it's performance on low moisture, ash percentages, suitable calorific value, low impurities ie Cl, Hg etc. To avoid operational issues, the Environmental Permit sets among other things, a list of accepted materials under the European Waste Catalogue (EWC) which can be treated. Under the Environmental Permit the operator shall demonstrate compliance by having strict protocols in place for accepting and dealing with non-conforming waste, carrying out regular sampling and monitoring analysis to assess compliance with their outputs including ash and emissions. Figures 7 A till D lists critical parameters of environmental compliance as instructed by the Environmental Permit.

When the waste arrives at the facility either by rail or road it is transported to the Tipping hall by vehicles taking into account transportation costs. The Tipping Hall is normally enclosed with Roller Shutter Doors to minimise nuisances while the air from the waste bunker is extracted for its use as a secondary air in the combustion process. The Tipping Hall encompasses a Traffic management system for the smooth operation of waste tipping. The disposed waste contained within the waste bunker gets mixed by the use cranes in a way that feedstock is homogenized for subsequent feeding to the chutes. Thereby, waste is fed to the moving grate with the aid of the feeding table. Figures 8 A till F highlights various parts and stages of the waste treatment process. The cranes as well as other critical parts of the plant are spares, redundant on standby mode to ensure the stable and

uninterrupted plant operation in case of a failure. Figure 9 presents the master and slave function of SNCR, which is a critical part of the Boiler for the NOx abatement.

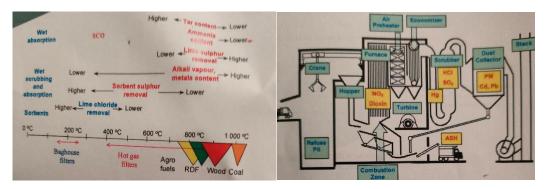


Figure 6 Range of various feedstock combusted at different Temperatures, hazardous pollutants generated at different stages of the plant and treatment technologies

quantity	
Waste code	Description
15 01 06; 15 03	02 Waste Packaging Mixed packaging: Absorbents, filter materials, wiping cloths and protective clothing, but only the fraction that is contaminated or can not be practically recycled or reused and would otherwise be destined for landfill.
19 05 01	Waste from aerobic treatment of solid wastes Non composted fraction of municipal and similar wastes, but only the fraction that is contaminated or can not be practically recycled or reused and would otherwise be destined for landfill.
19 06 04	Waste from anaerobic freatment of wastes Digestate from anaerobic treatment of municipal waste, but only the fraction that is contaminated or can not be practically recycled or reused and would otherwise be destined for landfill.
19 12 01; 19 12 07; 19 12 08	Wastes from mechanical treatment of waste Paper and cardboard; Wood other than mentioned in 19 12 06* and textiles, but only the fraction that is contaminated or can not be practically recycled or reused and would otherwise be destined for landfill.
20 01 01; 20 01 08; 20 01 10; 20 01 11; 20 01 38; 20 01 39	Municipal Wastes Paper and cardboard; Biodegradable kitchen and canteen waste; clothes; textiles; Wood other than mentioned in 20 01 37*; Plastics, but only the fraction that is contaminated or can not be practically recycled or reused and would otherwise be destined for landfill.
20 02 01	Garden and Park wastes Biodegradable wastes, but only the fraction that is contaminated or can not be practically recycled or reused and would otherwise be destined for landfill.
03 01; 20 03 ; 03 03; 20 03	Other municipal wastes Mixed municipal waste; Waste from markets; Street-cleaning residue Bulky waste;

Figure 7 A List of acceptable waste indicated by the Environmental Permit including RDF and other waste fractions and other waste

fractions ie digestate. Additional measures shall apply ie for the fractions contained in the mixed MSW under Chapter 20 of the EWC which might pose operational hazards. An example might be the bulkies which would require additional treatment such as shredding.

Parameters, for which reports shall be made below.	, at accordance with con	distante or end permit and					
Table S5.1 Reporting of monitoring data Forameter							
	Emission or monitoring point/reference	Reporting period	Period begins				
Continuously monitored emissions to air of SQ2, total organic carbon, NOX, HCI, particulate, CO and NHs , continuous monitoring as required by condition 3.6.1.	A1 [(point A1 on plan provided in pre-operational condition PM16)	Every 3 months	From the first date that waste is burned in the installation				
Extractively sampled emissions to air of SO <sub>2</sub> , total arganic carbon, NOx, HCI, particulate and CO, periodic monitoring as required by condition 3.6.1,		Every 6 months	From the first date that waste is burned in the installation				
Emisions to air of HF, NyO, Cd/TI, Hy, Sb. As, Pb, CY, Co, Cu, Mn, Ni, V and Their compounds (fota), dioxins/ Kurans (HEQ), dioxin-like PCS5 (WHO-TEQ Humany) Mammais), dioxin-like PCBs (WHO- TEQ Bith), dioxins/livens (WHO-TEQ Bith), dioxins/livens (WHO-TEQ Rish), dioxins/livens (WHO-TEQ Rish), dioxins/livens (WHO-TEQ Rish), dioxins/livens (WHO-TEQ Rish), dioxins/livens		Every 3 months for the first year of operation, and every 6 months thereafter.	From the first date that waste is burned in the installation				
Exhaust gas temperature, pressure, axygen content, water content and flowrate, continuous monitoring as required by condition 3.6.1		As requested by Agency site inspector. See Note 1.	From the first date that waste is burned ir the installation				
Furnace chamber temperature continuous monitoring as required by condition 3.6.1	Furnace PCC	As requested by Agency site inspector. See Note 1.	From the first date that waste is burned i the installation				
Wind speed and direction continuous monifoling as required by condition 3.6.1	Installation	As requested by Agency site inspector. See Note 1,	From the first date that wast is burned the installatio				
OI of bottom ash as required by condition 3.6.1	Bottom Ash	Monthly for the first year of operation, and quarterly thereafter.	From the				

Figure 7 B Environmental monitoring parameters under the Environmental Permit

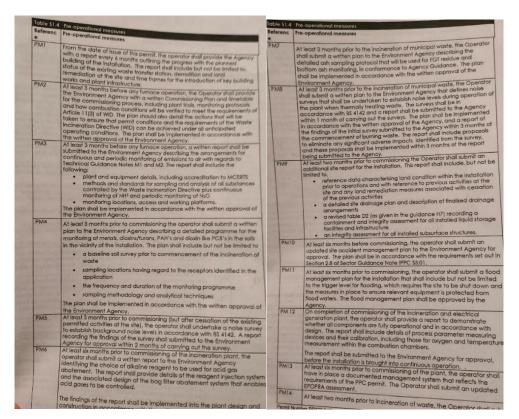


Figure 7 C Pre Operational conditions set under the Environmental Permit

Keleronc	Improvement programme regularments	No. of Concession, name	Reference	3 Improvement programme requirements Requirement		
CI		Date		requirement	Dote	
	The Closenstor shall provide the Environment Agency with a written pain commissioning report for approval, which shall include but not be initial or a D review of the performance of the facility against the conditions of this performance. If the facility against the conditions of this performance of the service and althab of the optimization of the environ abotesment systems, including: primary control measures for HDs formation, in perfordure control measures for HDs formation, in performance, reagent dowing roles in reagent dowing for acid gas abstement reagent dowing for acid gas abstement reagent dowing for acid such heavy restel abotement reagent dowing for acid such heavy restel abotement such as the such reagent dowing the reag	the Agency within 4 e months from the completion of the commissioni ng process, os defined by The Commissioni ng Process, os defined States		The operator shall prepare a written report detailing the relationship between conduction parameters (temperature, Or and flue gas flow rate) with CO and IOC concentrations that dates have the conduction parameters can be used under obtain how the conduction parameters and the empty and takes given is forward a date of the empty and be submitted to the Environment Agency for approvel. The report that be submitted to the Environment Agency for approvel.	ng Plan. Report to be submitted to the Agency within 4 months from the completion of the commission ng process. as defined by the Commission	
	<ul> <li>calibration reports for the continuous emissions manifolding sequement.</li> <li>verification of the fing of the outliery barners in response to falling temperature in the combustion chamber.</li> <li>verification that combustion conditions of the timoce comply with the minimum operating conditions in Article 6 of the WD, ore adequately monifored and controlled, and that sofe operating conditions in ensured and emissions are minimized.</li> <li>details of procedures developed during commissioning for achieving and temportariting calification process control and the conditional soft operating controlled by the achieving and temportariting califications process</li> </ul>		105	The operator shall prepare o withen report detailing the measures to be taken to ensure that under abnormal operating conditions relating to a failure of the porticuides. CEM, the emission find value for particuides given in Schedule 4 Table 5-11 (git) compliate with the report shall be ulumitied to the Environment Agency for approval. The report finding who be implemented by the operator from the date of approval in willing by the Agency.	ng Plan. Report to be submitted to the Agency within 4 months from the completion of the commissioni ng process, as defined by the Commissioni ng Plan.	
KC1	The Operator that prepare a written report that demonstrates that the Continuous Emission Marilon have been appropriately satisfacted and their posteriorance verifies to 82 EN 14181, for the relaces points and postmeters as position in Schedule 4 Table 54.1. The report that include the maximum undertaken and the results obtained, and be submitted in writing to the Environment Agency for approval.	Report to be submitted to the Agency within 3: months from the completion of the commissioni ng process, as defined by the Commissioni ng Pian.	IC6	The Operator shall subtril a willen proposal to the invironment Approxy to any our lasts to determine the size altitudine of the particulate matter in the subcast gas emissions to of them emission point AL. The proposal shall include methods for identifying the fractions within the PMus. Muss and PMu samps and a threadball to carry our bush field and produce a willian report on the results. On receipt of willian approvality the Agency for the proposal and finantable, the Operator that carry out the tests and submit outfram report to the Agency that includes the results of the tests.	Proposals to be submitted to the Agency within 6 months of the completion of commission ng as defined by the commission	
	The Operator shall undertake a study and produce a withen report to verify that haldsmine time, minimum temperature and angen content of the transition goes in the formation present the With angewenning to the transition of the time anticipated most underview present expending conditions. The server that be submitted in writing to the Environment Agency for approval.	Report to be submitted for the Agency within 3 months from the completion of the completion of the commissioni or geocoles, as defined by the Commissioni		The Operator shall review the potential techniques for confinuous measurements for heavy metado, PAH's closine? Inaras and down-like PCBs. The eview includie indicate cost, availability, accuracy and detection fimits. A written report of the review shall be submitted to the Environment Agency	ng Plan. Report to t submitted the Agen within manths fro the completio of commissio ng proc as defi	

Figure 7 D Improvement Conditions set under the Environmental Permit.



**Figure 8A** A view inside the Tipping hall area encompassing a Traffic Management System linked to appropriate unloading bays with raised kerbs. The unloading of waste is assisted by the traffic controller system thereby instructing drivers when and where to unload waste. Vehicles are directed to the appropriate bay using traffic light indicators.

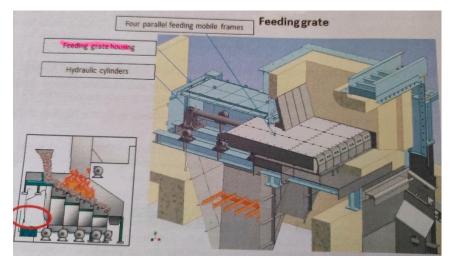


Figure 8B Feeding table parts

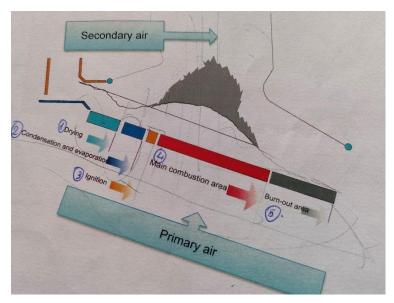


Figure 8C Combustion process at different zones

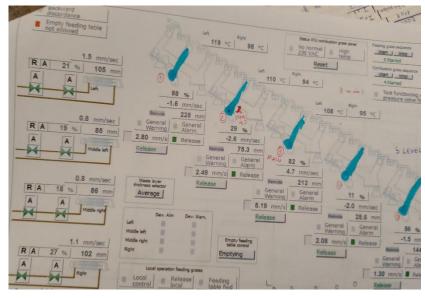


Figure 8D DCS interfaces of grate movement

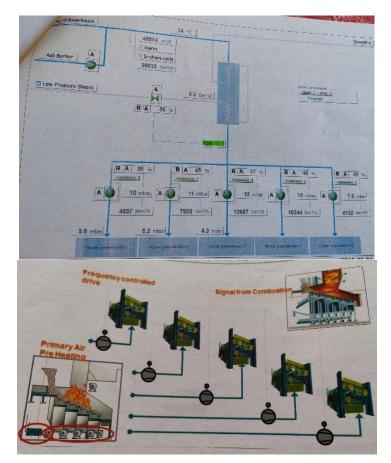


Figure 8 E1 Feeding grate primary air supply and DCS screen

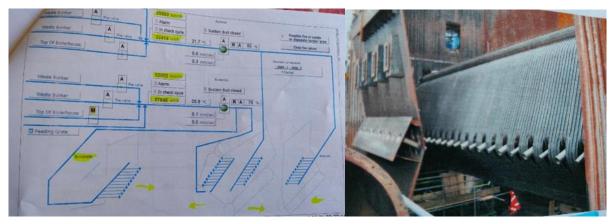


Figure 8 E2 Feeding grate secondary air supply and DCS screen

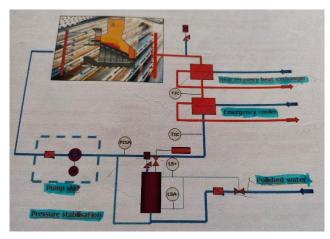


Figure 8 F Water Cooling system

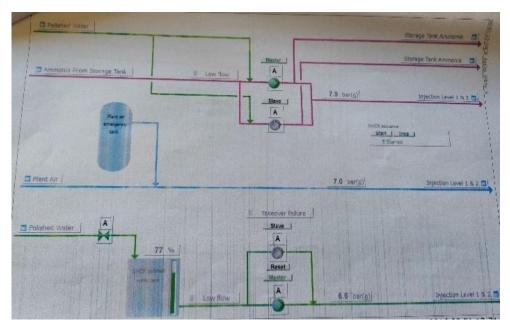


Figure 9 Master and slave function of NOx abatement SNCR system

Auxiliary Burners are in place to ensure the smooth plant operation. Figure 10 highlights the use of Auxiliary Burner. Their operation particularly when starting, stopping and in case of malfunctioning ensures that the plant shall stay compliant with the rule of 850C for 2 seconds according to 2010/75/EU. The waste on the grate is moved in a way that allows the waste homogenization, at the appropriate speed, thereby monitoring the thickness of layer adjusting speed. The waste will be excelling to the different zones of drying on the top, ending up burned out at the bottom of the grate where the ashes are disposed. The conditions of complete combustion are achieved with the supply of preheated air in excess. This is ensured by the addition of preheated air below the grates (Primary Air) and above the boiler prism (Secondary/Tertiary Air). This system ensures the avoidance of formation of potent gases including Carbon monoxide, dioxins, furans. By means of a non-catalytic SNCR reactor present at 2 levels of the Boiler area and with the use of appropriate features encompassing adequate lances, ammonia or urea is injected. In this way, NOx formation is inactivated to form Nitrogen within the appropriate temperature range before the 1st pass of the steam boiler. Figures 11 A, B and C present the SNCR system process.

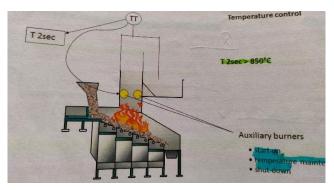


Figure 10 Auxiliary Burners location

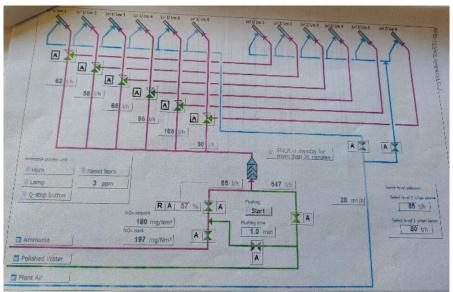


Figure 11A DCS SNCR dosing system layout



Figure 11B SNCR dosing system, lances and associated features

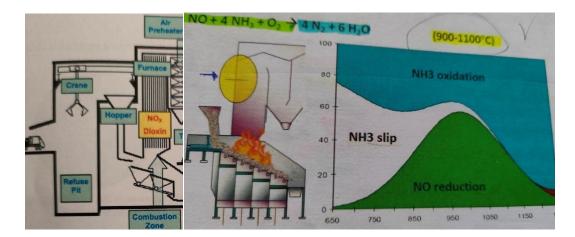
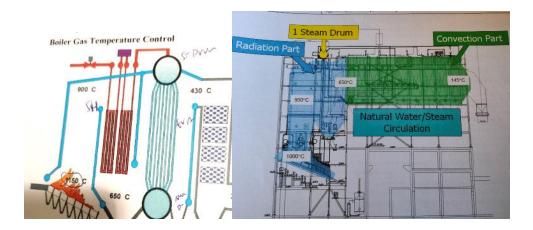


Figure 11 C NOx formation, SNCR System tackling NOx emissions at the appropriate Temperature and with the right dosage to be verified by CEMS monitoring performance

The steam boiler (ie 87MWt) is designed in such a way that by the flue gas turbulent motion and subsequent movement inside the empty passes; from the 1st to the 3rd passage, changing gas direction, heavier particles of fly ash are expelled while on the same time the flue gas Temperatures decreases to protect the heat exchanging parts. The flue gas passes on the 4th pass exchanging heat, with the heating tubes in the convective part section at the right Temperature range. The water and steam separation takes place inside the boiler drum where levels of water are monitored and triggered by alarms. Water level normally stays in the middle. The water and steam fractions are continuously recirculated inside the Boiler in a way that impurities are removed by a Blow Down valve to the mud drum and renewed demineralised water is fed into the system. Figures 12 A till D depict main Boiler parts and their functions.



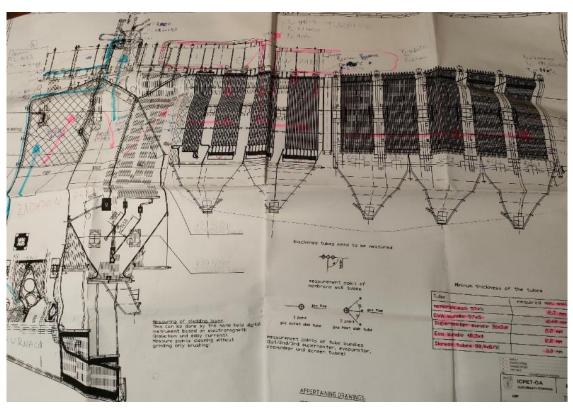


Figure 12 A Indicative Temperature operational ranges within the Boiler.

Figure 12 B Main parts and sections of the Boiler

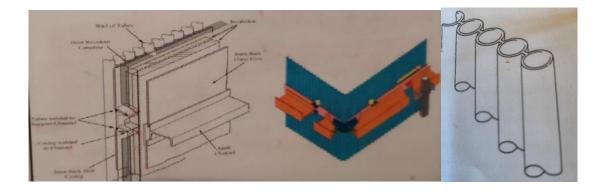
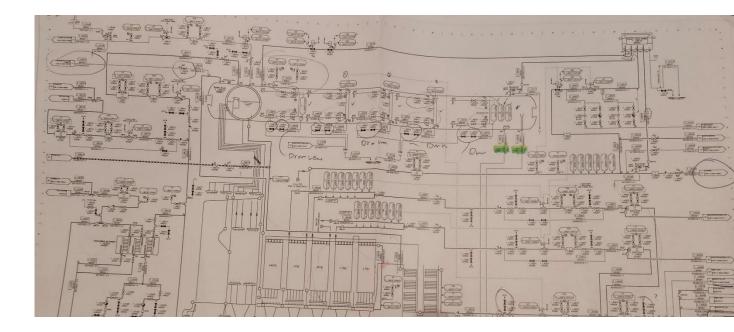


Figure 12 C Boiler membrane wall tubes



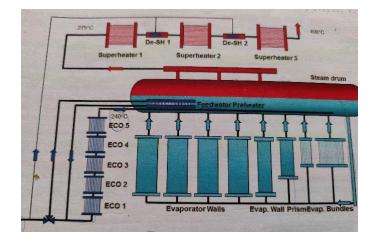


Figure 12 D Boiler steam separation fed to Superheaters

The wastewater is reused to cool the ash. Figure 13 presents the ash conveying system. Water quality is monitored continuously in sample stations to ensure compliance at different stages of the plant so that it meets compliance thresholds with EN 12952-12 ie to be free of salts having suitable conductivity, pH, to be free from dissolved gases such as O2. Treatment is carried out at different stages of the plant to reach the appropriate quality protocols with various means including but not limited to activated carbon filters, ion exchange resins, with chemical addition including ammonia, trisodium phosphate dosage and the use of a deaerator for the separation of dissolved gases. Figures 14A to C shows areas of the water treatment process.

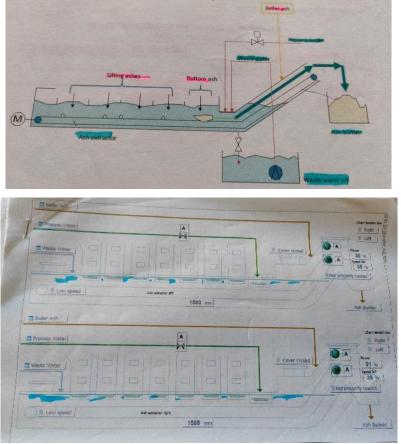


Figure 13 Ash conveyor system



Figure 14A Areas of wastewater treatment process

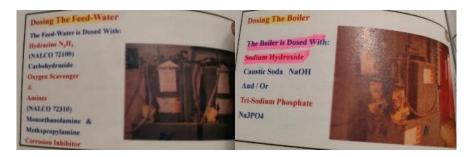


Figure 14B Water dosing chemical treatment



Figure 14C Boiler Cleaning of dissolved gases with the use of deaerator

The superheated steam ie approximately 100 t/hr per boiler from the 2 steam boilers is delivered from the superheater tube bundles. In the Superheaters section the steam reaches in optimal conditions (52 bar, 400C) and fed to the Turbine. The Superheaters are supported by attemperators which are been used to cool down Temperatures as well as to protect the lifespan of Superheater bundles. The superheated steam in the turbine expands and drives the generator to produce electricity of roughly 25% of the total energy load in an ERF plant. The rest of the usable steam is extracted from the Turbine via pipework to nearby facilities or for purposes of district heating and the remaining usable steam to cover the internal operation requirements. Figures 15 A to C highlight the Turbine operation.

The steam gets condensed and driven to cool down by means of cooling such as cooling towers where steam is condensed, water is processed and returned to the feeding system. The entire system works in an optimum energy efficiency manner using steam recirculation. Figures 16 A and B focus on the steam cooling system. Figure 17A pinpoints the Turbine steam extraction parts while Figure 17B demonstrates how the whole steam cycle works.

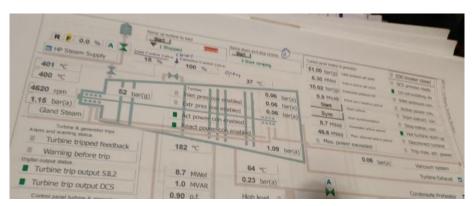


Figure 15A DCS layout of Turbine functions and alarms



Figure 15 B Steam expansion inside the Turbine

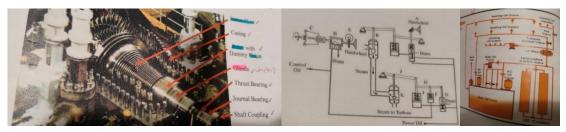


Figure 15 C Turbine main parts and supporting features

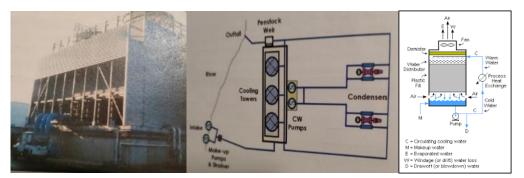


Figure 16A Cooling Tower working principle and cooling process

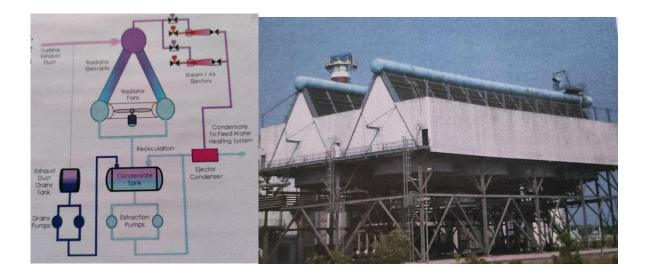


Figure 16 B Air Cool Condenser working principle and cooling process

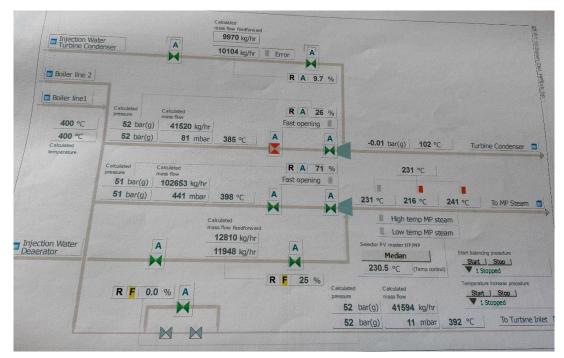


Figure 17A Turbine extraction parts

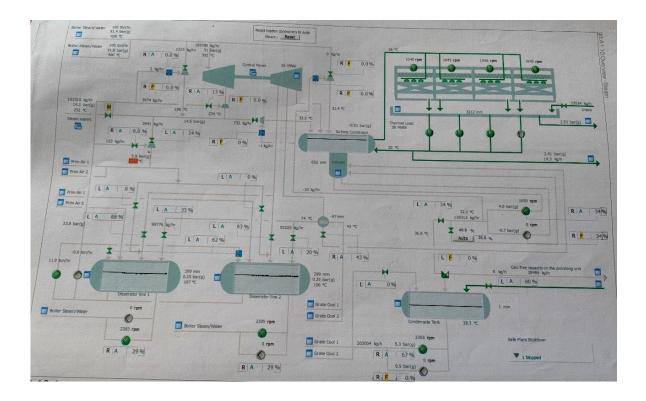


Figure 17 B DCS illustrating main parts of the steam cycle process

The formation of soot is driven mainly by the high operating Temperatures from combustion and the acidic environment by the acid gases formed inside the boiler. Figures 18A to C indicate the mechanisms that cause boiler tube failures and their associated effects. Frequent cleaning of steam boiler with the means of shower cleaning cycles in the 2nd/3<sup>rd</sup> passage or rapping cycles on the heat exchangers horizontal part, sometimes are not on their own sufficient. Figures 19A to C highlight the means of boiler cleaning.

The constant monitoring of performance including the flue gas path, monitoring Temperatures including the convective part in combination with the steam production flow is vital. It sometimes requires rigorous response by the operator unblocking ash bridges with the use of pressurized equipment especially on the 2/3 pass of the boiler. The ash deposits end up through a closed circuit ie double flap valves and rotary valves system, on the ash extractor and meet with the bottom ash at the bottom side of the grate and from there in the IBA ash storage bunker. Figure 20 shows how the ash is transported to the ash extractor and to the ash bunker. From the bunker with the use of slag handling cranes ash is loaded to trucks. The ash accounts for approximately 20 to 25% of the total waste throughput. The ash is regularly sampled as part of its disposal and is subject to regular laboratory analysis monitoring.

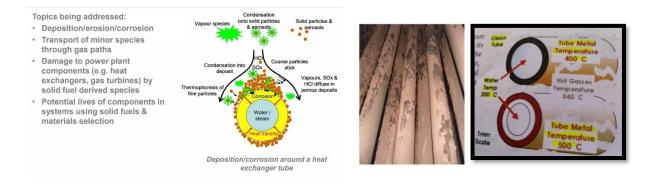


Figure 18A Root causes of boiler tubes failures including scale inside the heat exchanger and deposits condensation around the heat exchanger tube



Figure 18B Boiler tubes thinning, scabbing, O2 attack, pitting, Flow Accelarated Corrossion and cracking



Figure 18 C 2<sup>nd</sup> and 3<sup>rd</sup> part boiler ash formation causing blockages

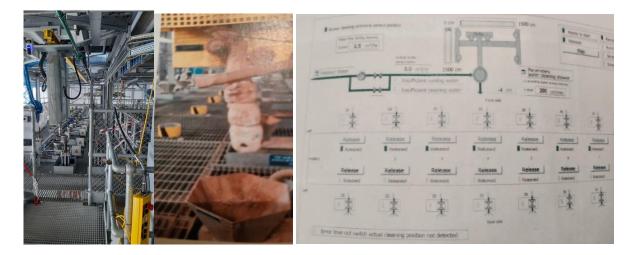


Figure 19A Boiler shower cleaning process and DCS layout screen



Figure 19B Boiler rapping system and DCS layout screen

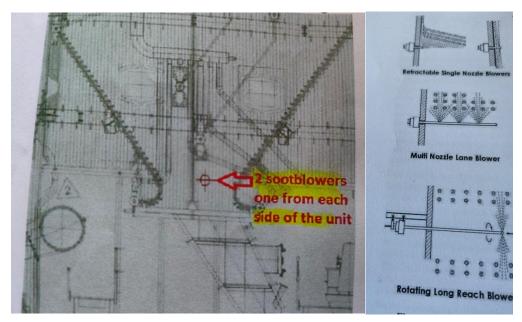
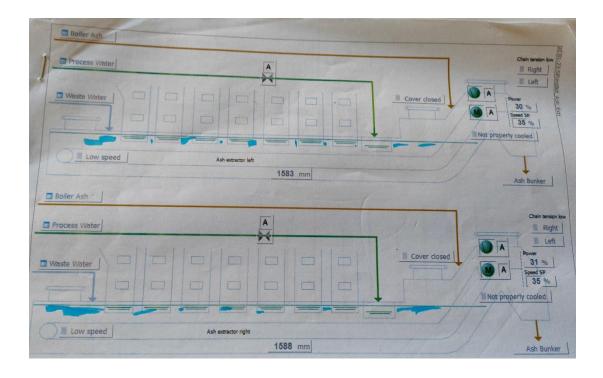


Figure 19 C Sootblower system



**Figure 20** Fly ash from the 2<sup>nd</sup> and 3<sup>rd</sup> pass and the horizontal heat exchangers part is extracted to the ash extractor

The flue gas after leaving the economiser bundles where it receives heat to heat up the water, the gas exits from the boiler tail end to a system called Flue Gas Treatment (FGT) with the assistance of an ID Fan under slight negative pressure. The FGT system is insulated by lagging and trace heated to avoid Temperature drop. Each FGT Line system could consist of 2 venturi scrubbers with 2 lime silos, 1 Pulverised Active Carbon (PAC) silo in two stages and a bag filters system encompassing a compressed air pulse cleaning system and a screw conveyor for the Air Pollution Control residue (APCr) removal. In the venturi scrubber section, hydrated lime is fed with hoses in both stages and is recirculated and reused to deal with acid gases such as HCl, HF, SOx. Additionally, PAC is fed to a stage reactor for the reduction primarily dioxins and furans that could be reformed from flue gas cooling, but also other contaminants including heavy metals ie Hg. The purified flue gas is continuously monitored by CEMS operation to stay well below thresholds and comes of the stack at dispersion speed flow, while the APCr disposal is subject to legal monitoring surveillance as it contains potential hazardous and toxic compounds. The APCr leaves the plant in enclosed vehicles. The APCr fraction accounts for roughly 3% of the total waste throughput. Figure 21 highlights the working conditions of the ID Fan, while Figure 22 the various options for acid emissions neutralisation using alkaline chemicals. Figures 23 A to F depicts the main FGT parts and their functions.

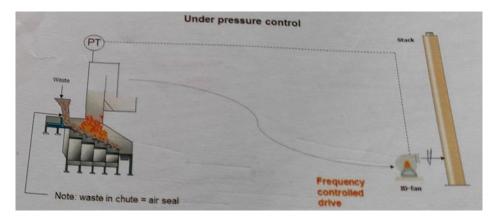


Figure 21 ID Fan working under slight negative Pressure to extract flue gas

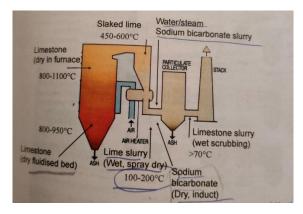


Figure 22 Different options to tackle acid gases

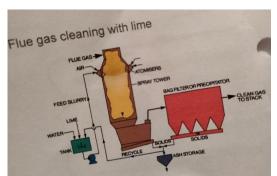


Figure 23A Hydrated lime spent is recirculated in the 2 stages Scrubber Reactor

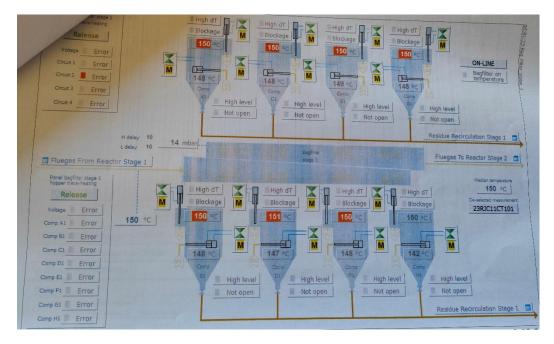
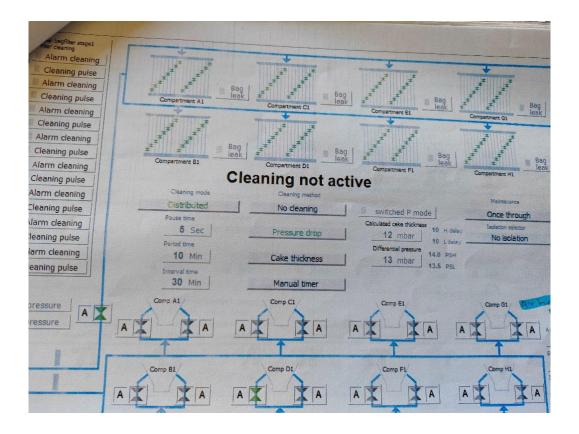


Figure 23 B DCS layout of Bag filters



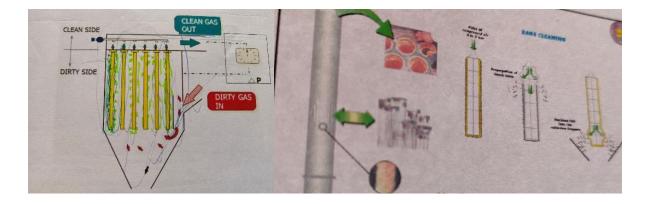


Figure 23 C Bag filters cleaning detected by Pressure difference with compressed air flush

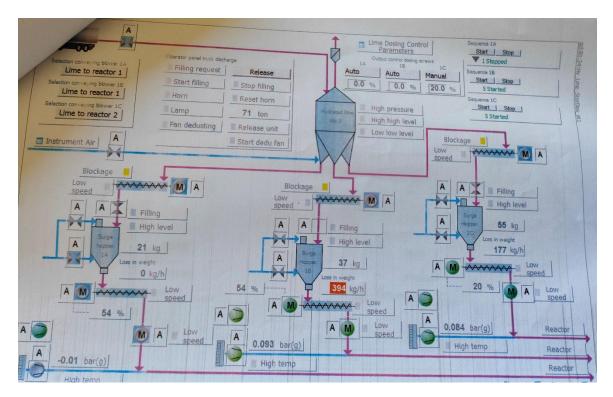


Figure 23 D DCS layout demonstrating the Lime dosing to the Scrubber reactor

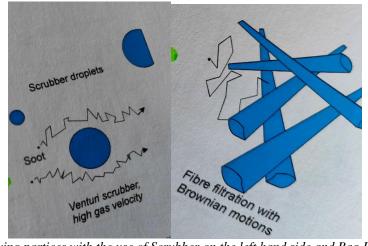


Figure 23 E Removing partices with the use of Scrubber on the left hand side and Bag Filters system on the righthand side

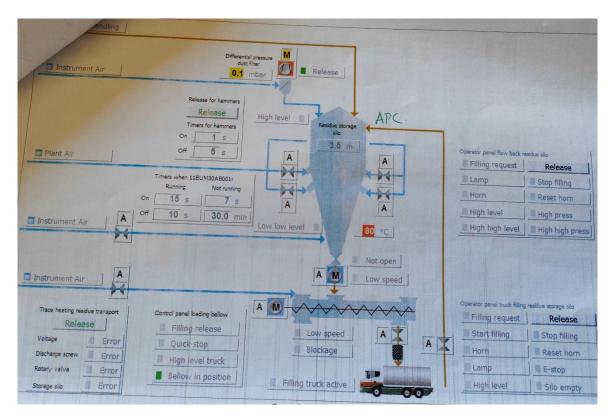


Figure 23F DCS layout unloading of APCr